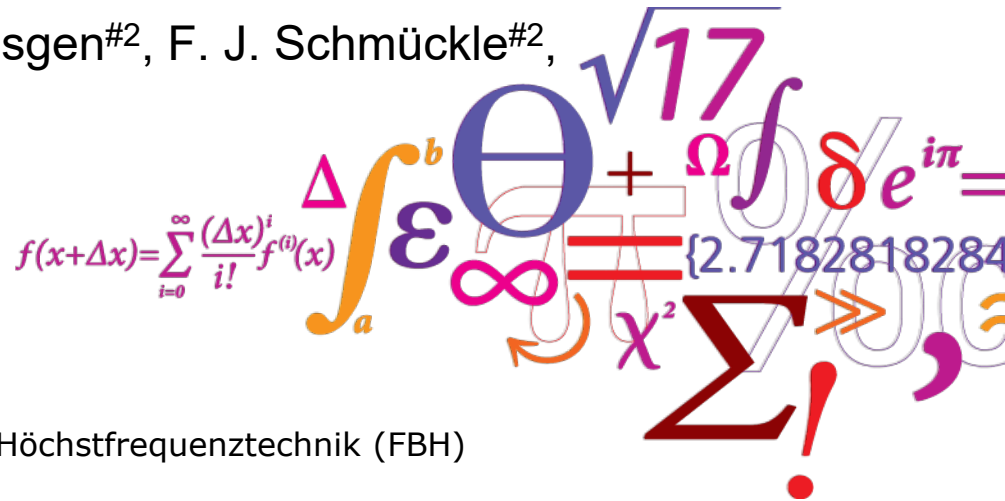


# Impact of Calibration Procedure on Sub-Millimeter-Wave Transistor Characterization and Modeling

T. K. Johansen<sup>#1</sup>, R. Doerner<sup>#2</sup>, T. Flisgen<sup>#2</sup>, F. J. Schmückle<sup>#2</sup>,  
W. Heinrich<sup>#2</sup>

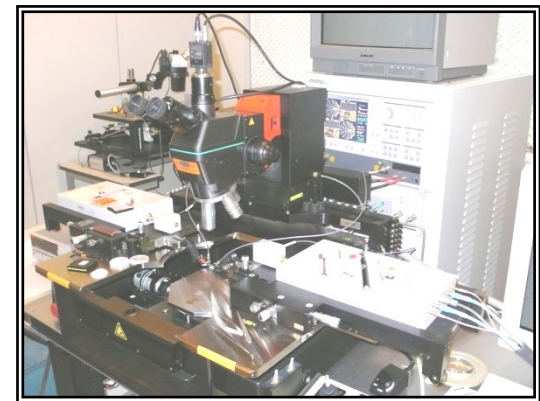
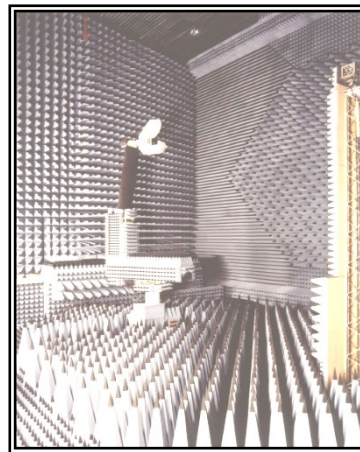
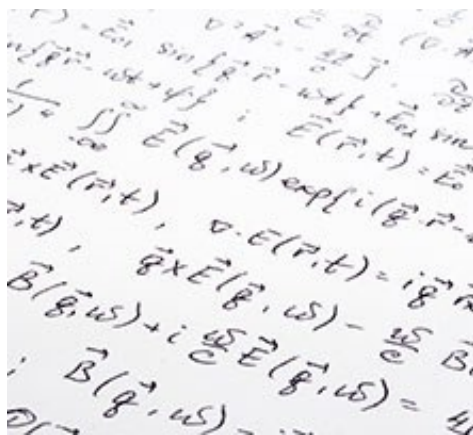
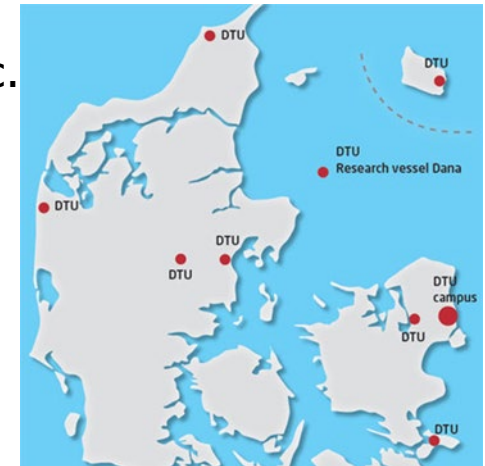
<sup>#1</sup>DTU - Department of Electrical Engineering  
Electromagnetic Systems Group (EMS).  
Technical University of Denmark  
Kgs. Lyngby / Denmark

<sup>#2</sup>Ferdinand-Braun-Institut - Leibniz-Institut für Höchstfrequenztechnik (FBH)  
Berlin / Germany



## About Technical University of Denmark

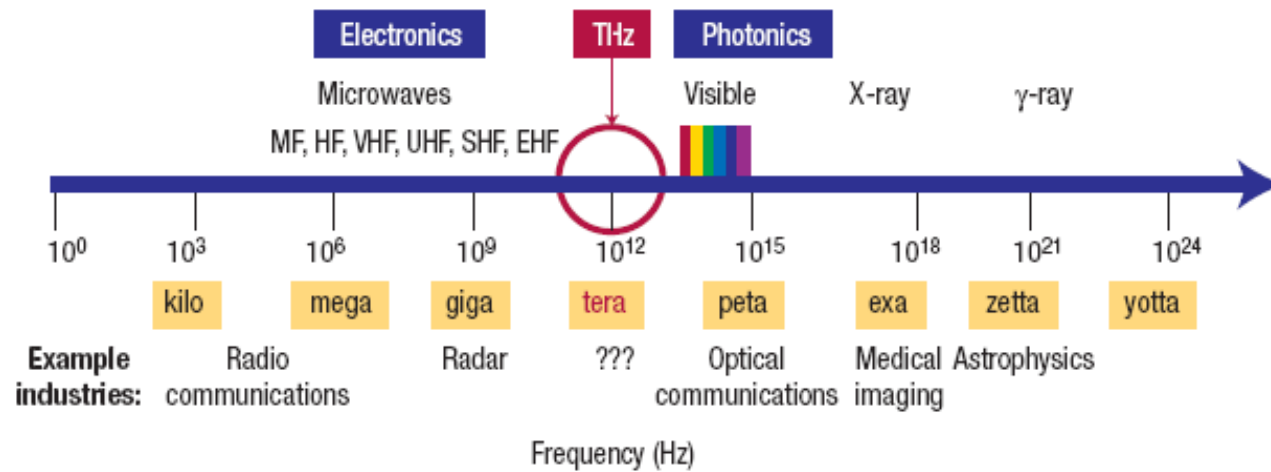
- Largest technical university in Denmark
  - Most engineering students: 11.200 B.Sc/M.Sc.
  - Around 6000 employees
- 18 Departments
  - Cover most engineering disciplines
  - From civil engineering to system biolog and mangement
- Department of Electrical Engineering
  - Electromagnetic systems group



# Outline

- Motivation: Sub-mm-Wave Applications
- Transferred-Substrate InP HBT Technology
- Characterization Issues for Downscaled Sub-mm-Wave Devices
- Calibration Issues Investigated by EM Simulation
- Summary

# Motivation: Sub-mm-Wave Applications



The part of the electromagnetic spectrum ranging from 100 GHz to 10 THz is largely unexploited and offers large unlicensed bandwidth for high resolution imaging, sensitive radars, broadband wireless communication, spectroscopy, material characterization, etc.

# Motivation: Sub-mm-Wave Applications

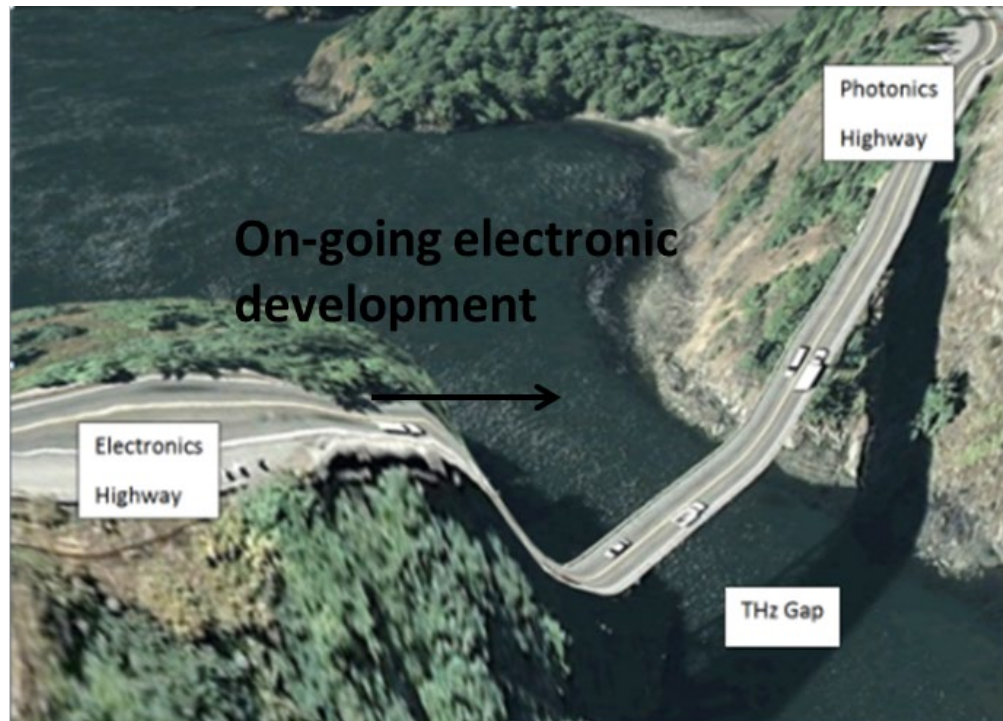
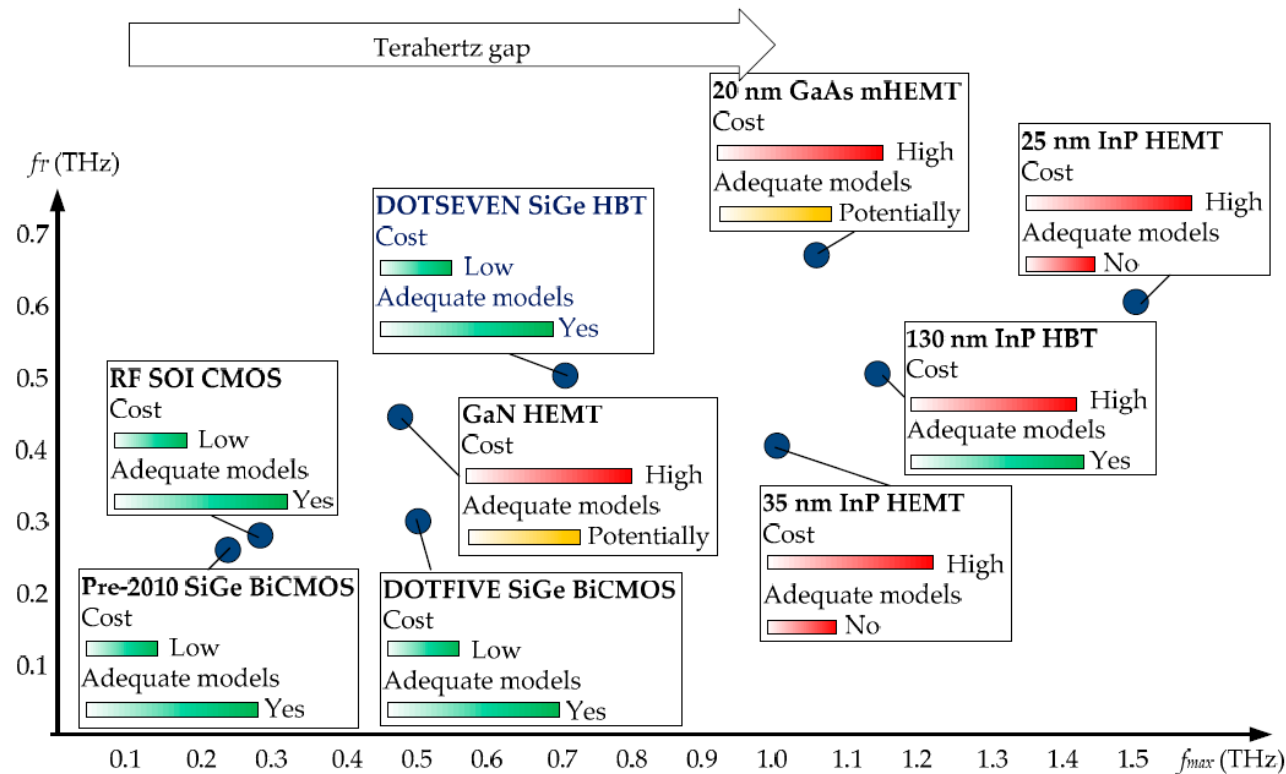


Image courtesy of CELTA ITN project (<http://www.celta-itn.eu>)

On-going electronic development towards low-cost, small-size and efficient signal sources to close the so-called "Terahertz Gap".

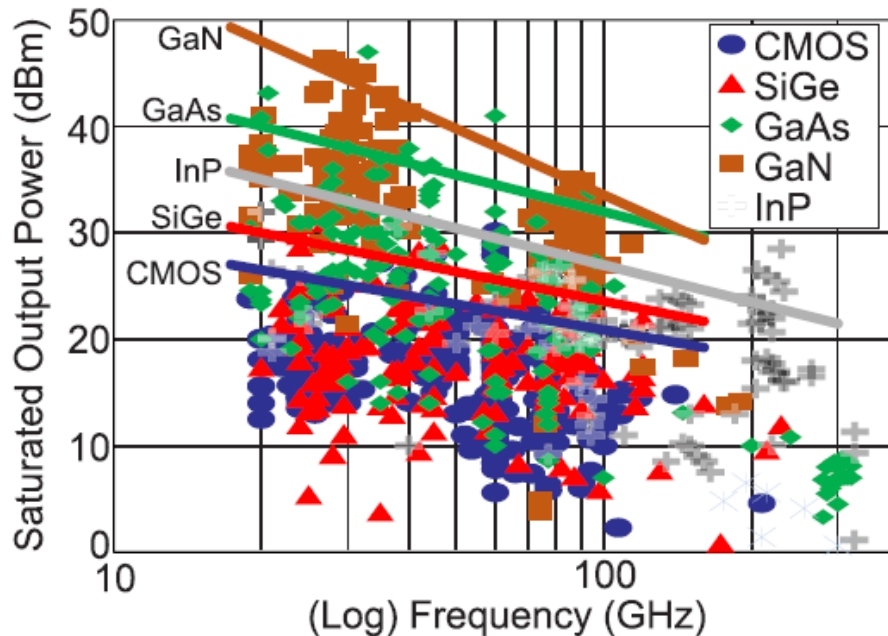
# Motivation: Transistors for Sub-mm-Wave Electronics



M. Bozanic and S. Sinha, *Sensors*,  
19, 2454, May. 2019.

# Motivation: Transistors for Sub-mm-Wave Electronics

Reported saturated output powers  
of power amplifier MMICs

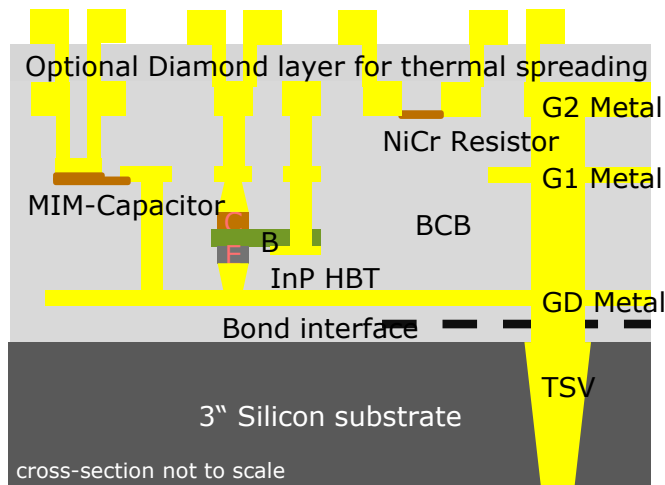


Of the various transistor families **InP** based transistors (InP HBT & InP HEMT) offer the best prospect for sub-mm-wave electronics

V. Camarchia et al., T-MTT,  
Vol.68, No. 7, July 2020.

# Transferred Substrate InP HBT Technology: FBH Development

FBH's transferred-substrate InP DHBT MMIC process targets high-power applications from mm-waves to sub-mm-wave frequencies....



Schematic cross-section of FBH's InP HBT transferred-substrate technology

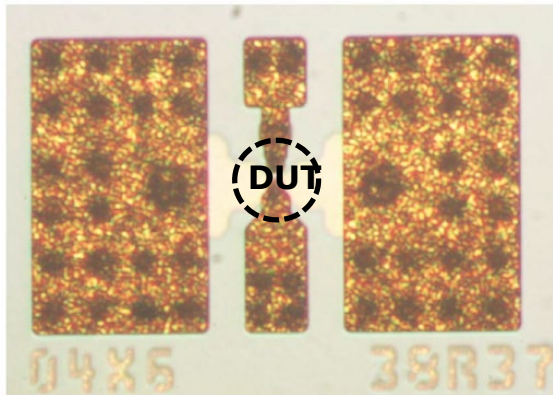
## Process specs [6]:

- 3 gold metal layers in BCB
- compatible to flip-chip and wire bonding
- thin-film resistors & capacitors
- transfer to Si-Substrate
- Optional thermal spreading layer with diamond
- TSV for substrate mode suppression
- 0.8  $\mu\text{m}$  node DHBTs with  $f_T/f_{max} \sim 350$  GHz and breakdown voltage  $> 4.5$  V

[6] N. Weimann *et al.*, "SciFab - a wafer-level heterointegrated InP DHBT/SiGe BiCMOS foundry process for mm-wave applications," *Phys. Status Solidi A*, vol. 213, no. 4, pp. 1244–1245, 2016.



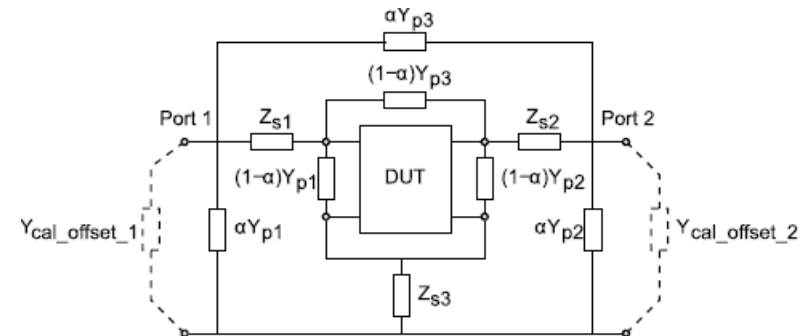
# Transferred Substrate InP HBT Technology: Best Case Using InP/GaAsSb DHBT



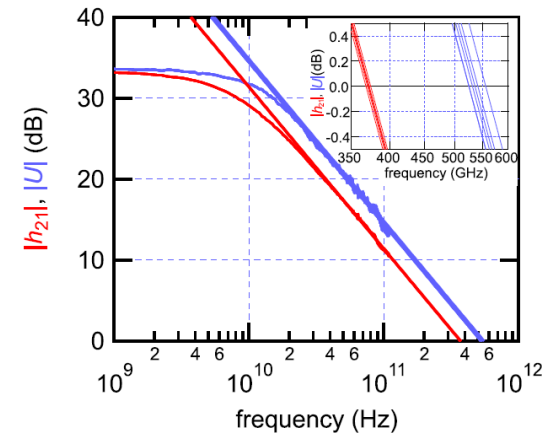
EXTRACTED UNITY-GAIN FREQUENCIES

	comp.	parameter $\alpha$			iterative method [3]	
		0.0	0.6	1.0	single pole	-20 dB/dec
$f_T$ (GHz)	no	368	370	371	373	370
	yes	374	372	371	376	373
$f_{max}$ (GHz)	no	541	531	524	540	525
	yes	555	535	524	545	531

N. Weimann et al., "Transferred-Substrate InP/GaAsSb Heterojunction Bipolar Transistor Technology With  $f_{max} \sim 0.53$  THz," IEEE Trans. Electron Devices, vol. 65, no. 9, pp. 3704–3710, Sept. 2018.



Deembedding network with compensation.



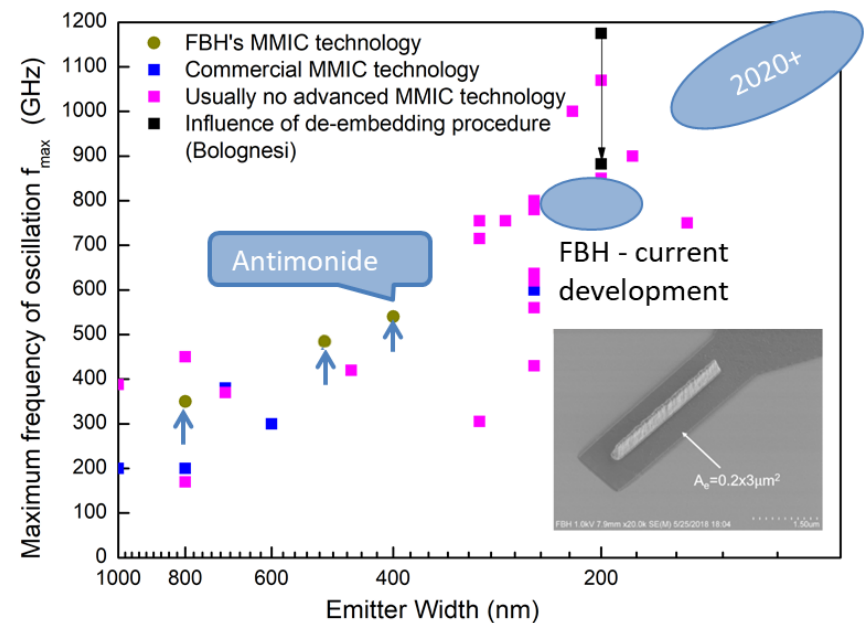
# Transferred Substrate InP HBT Technology: FBH Road Map

## Goal

- $f_{\max} \sim 500$  GHz with stepper technology
- $f_{\max} > 1000$  GHz with e-beam technology

## Approach

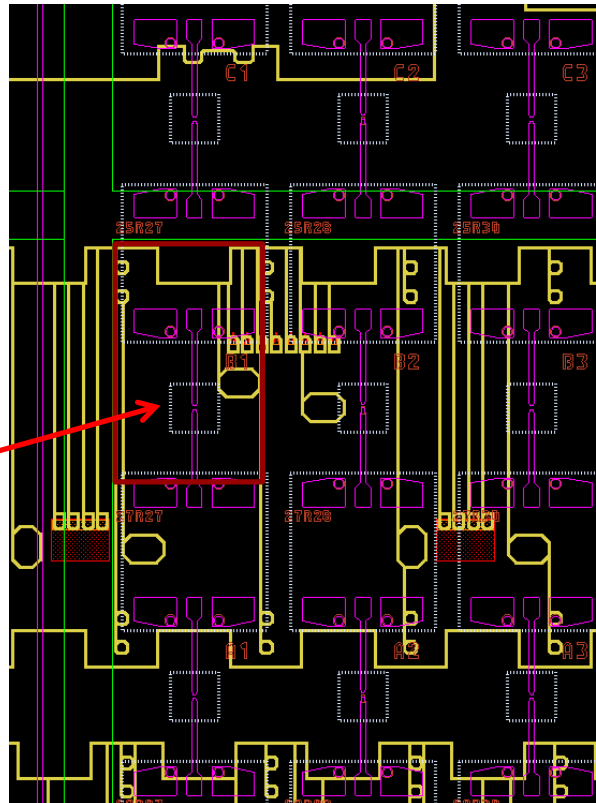
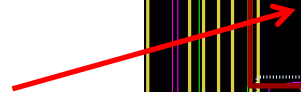
- Scaling to 100 nm
- Base contact optimization
- New Epitaxial structure
- Improved thermal properties with diamond



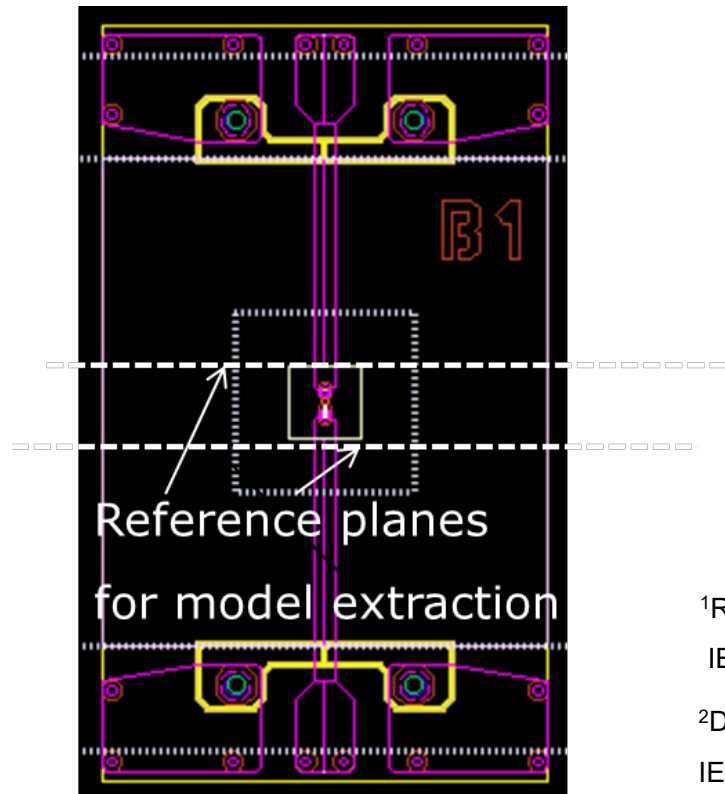
# Characterization of Sub-mm-Wave InP HBT Devices using Thin-Film Microstrip Line Test Structures

device-under-test:

$1 \times 0.3 \times 6 \mu\text{m}^2$  InP  
HBT type B1



# Setting the Reference Planes for Characterization



## Approach:

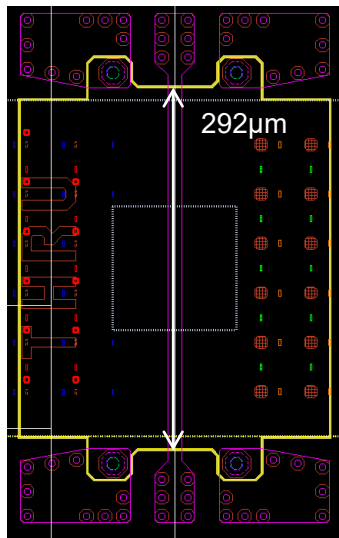
- On-wafer multilayer TRL (mTRL) calibration procedure to set reference planes directly at device terminals<sup>1,2</sup>
- Thin-film microstrip lines to avoid slot modes and other resonances
- $Z_0$  normalization using embedded resistor structure

<sup>1</sup>R. B. Marks, A Multilayer Method of Network Analyzer Calibration, IEEE Trans. Microwave Theory and Techn., July 1991.

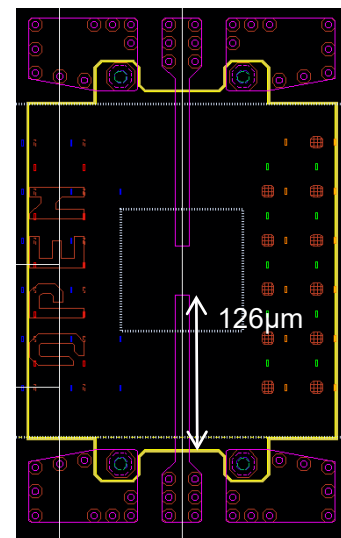
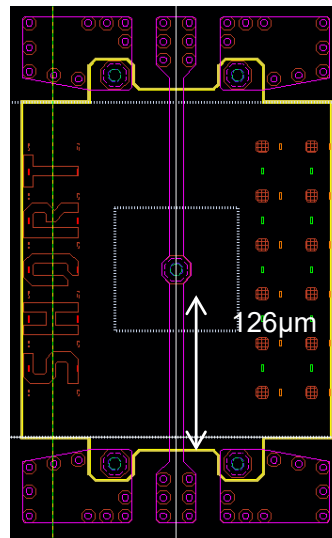
<sup>2</sup>D. F. Williams and R. B. Marks, Transmission Line Capacitance Measurement, IEEE Microw. Guided Wave Letts., Sept. 1991.

# On-wafer Multi-Line TRL Calibration Structures - I

Thru structure



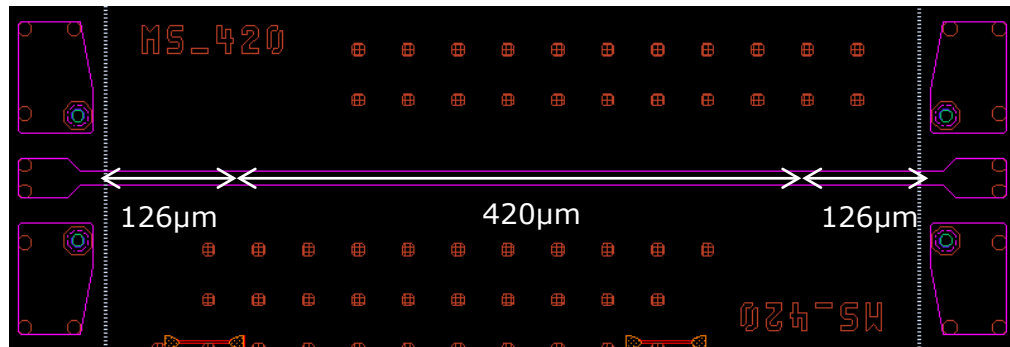
Reflect structures (use short or open)



It is seen that it would be meaningful to define the reference planes at a distance of 126  $\mu\text{m}$  from the pads and let the thru have a length of 40  $\mu\text{m}$ .

# On-wafer Multi-Line TRL Calibration Structures - II

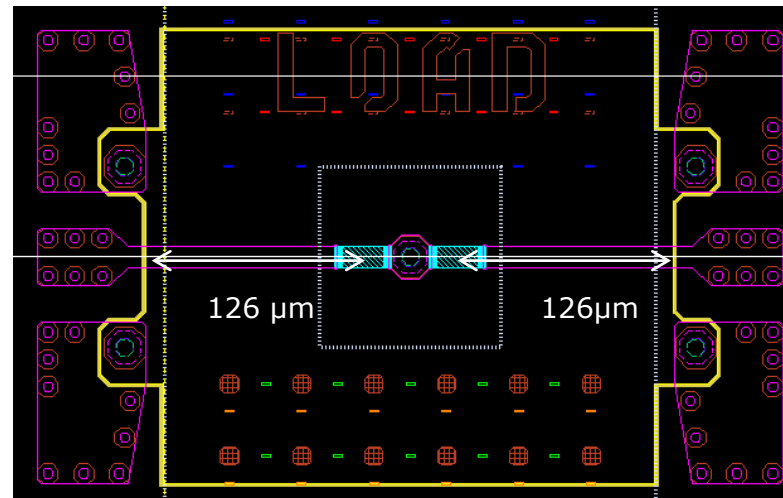
The reference planes for the line structures are all located at a distance of 126  $\mu\text{m}$  from the pads.



Line structures: (MS150), MS420, MS1250, MS1950, MS2850, MS8500

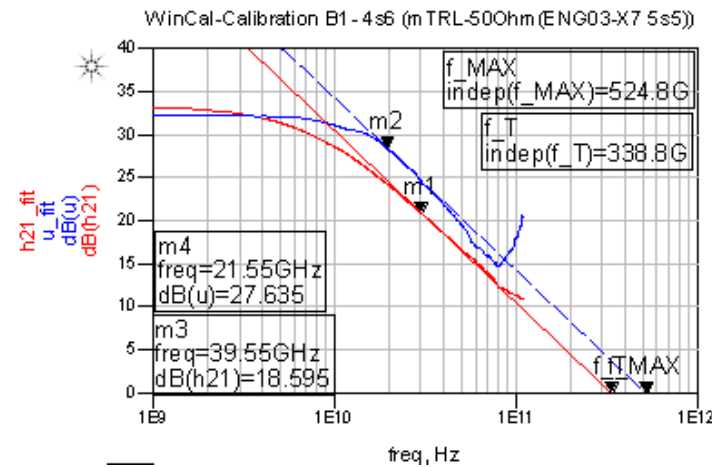
# On-wafer Multi-Line TRL Calibration Structures - III

Embedded resistor structure



This structure is used to estimate the capacitance per unit length and thereby to set the characteristic impedance  $Z_0$ .

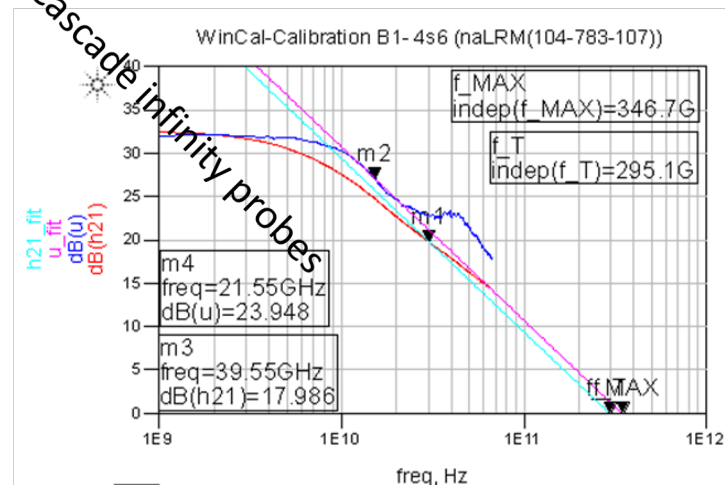
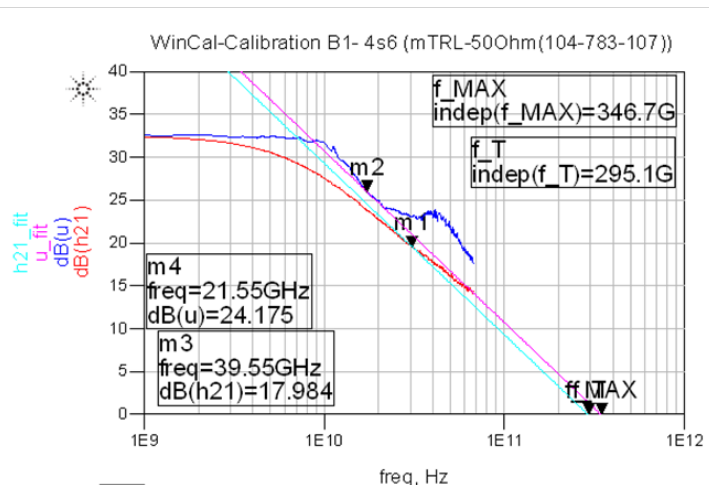
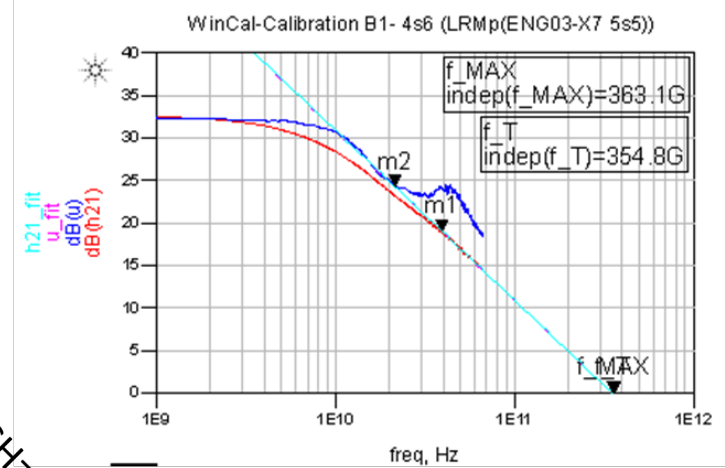
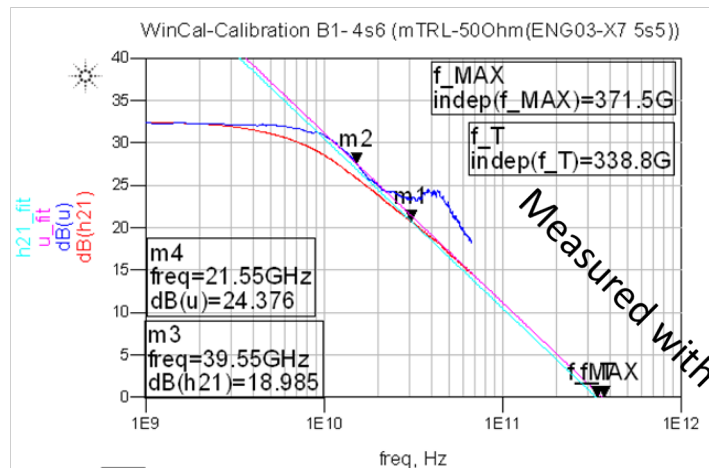
# Characterization of Downscaled Sub-mm-Wave InP HBT Devices



Measured with 110 GHz GGB pico-probes



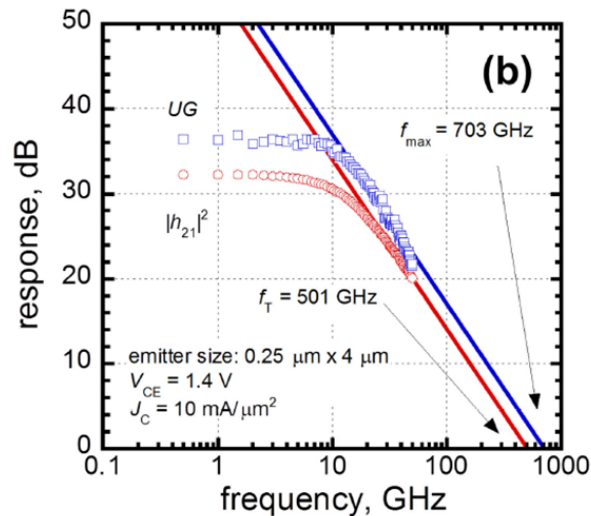
# Characterization of Downscaled Sub-mm-Wave InP HBT Devices



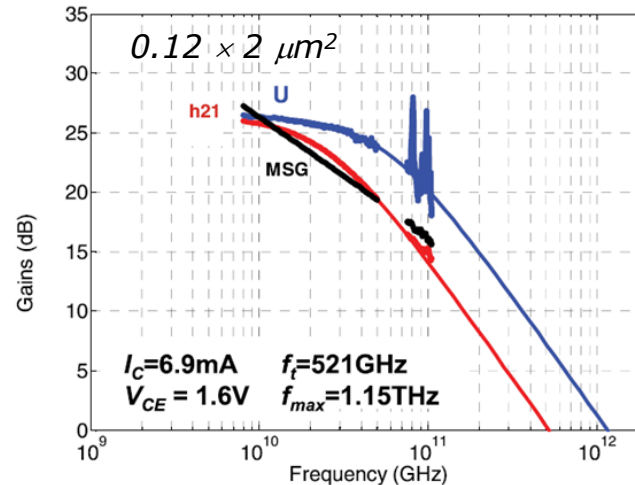
# Characterization of Downscaled Sub-mm-Wave InP HBT Devices

Other research groups report similar behavior!

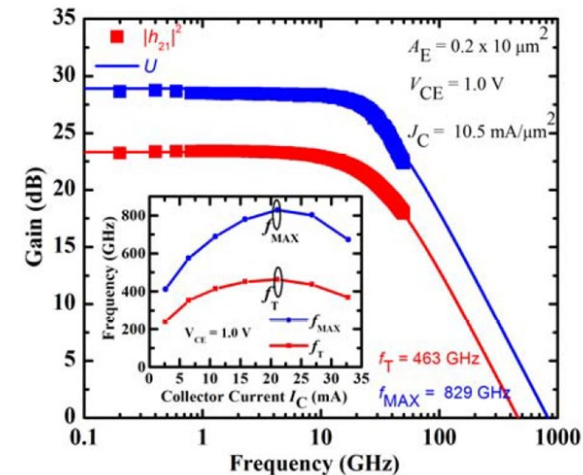
NTT<sup>1</sup>



Teledyne-UCSB<sup>2</sup>



ETH-Zürich<sup>3</sup>

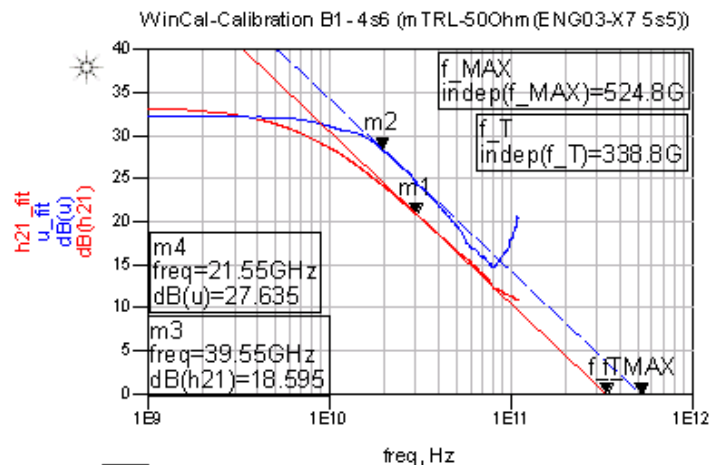


<sup>1</sup>T. Hoshi et al., IEICE Electronics Express, Vol. 16, No. 3, 1-6, 2019.

<sup>2</sup>M. Urteaga et al., Proceedings of the IEEE, Vol. 105, No.5, pp. 1051-1067, June 2017

<sup>3</sup>A. M. Arabhavi et al., IEEE BCICTS, 2018.

# Characterization of Downscaled Sub-mm-Wave InP HBT Devices



On-wafer probing creates strong ripple in Mason's gain:

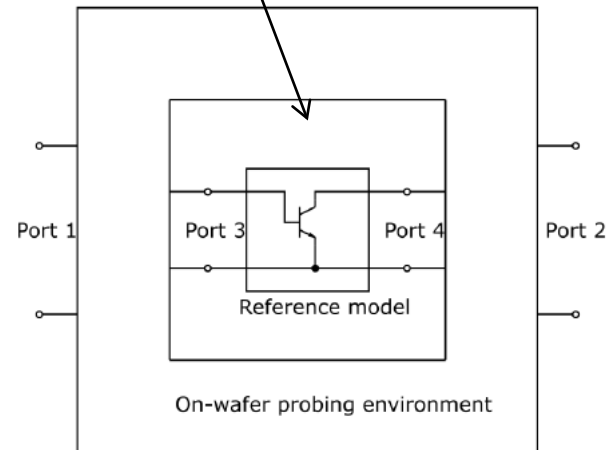
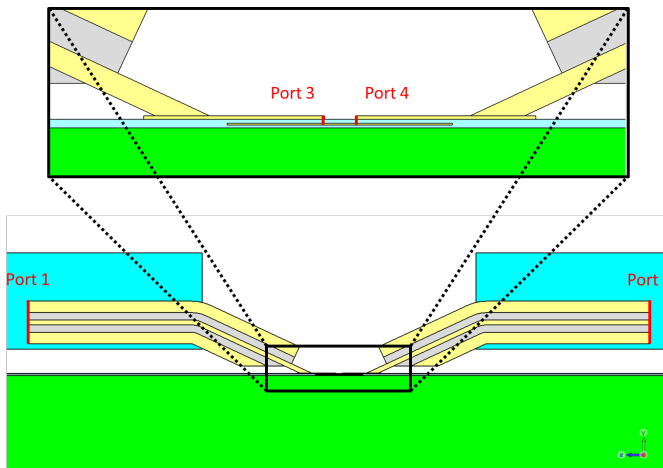
$$U = \frac{|(S_{21}/S_{12}) - 1|^2}{2k|S_{21}/S_{12}| - 2 \operatorname{Re}[S_{21}/S_{12}]}$$

$$k = \frac{1 - |S_{11}|^2 - |S_{22}|^2 + |S_{11}S_{22} - S_{21}S_{12}|^2}{2|S_{12}S_{21}|}$$

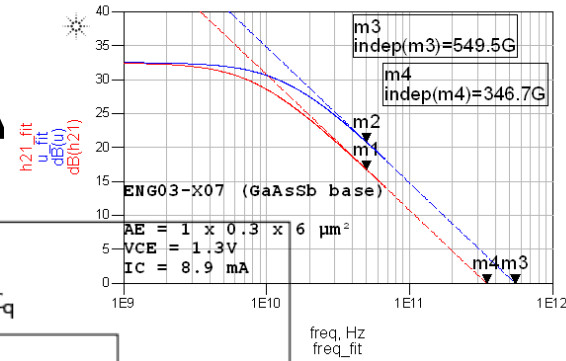
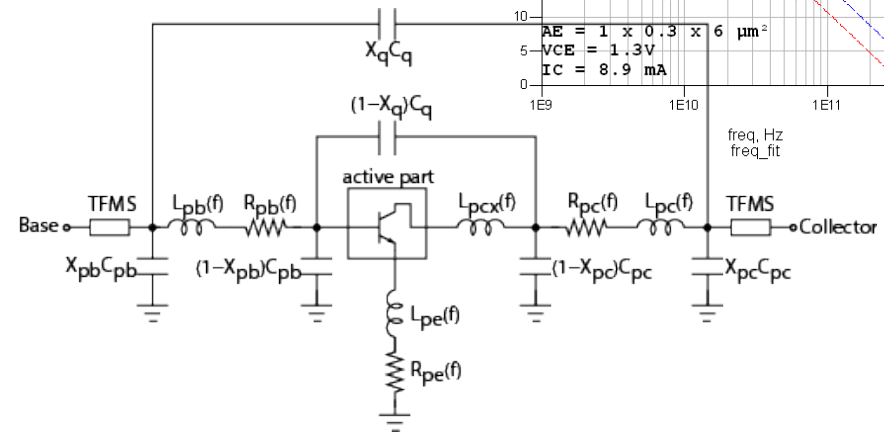
In agreement with literature this could be explained by increased influence from parasitic probe coupling effects in an on-wafer environment as the  $|S_{12}|$  of down-scaled devices is small and hence easily corrupted.

# Calibration Issues Investigated by EM Modeling

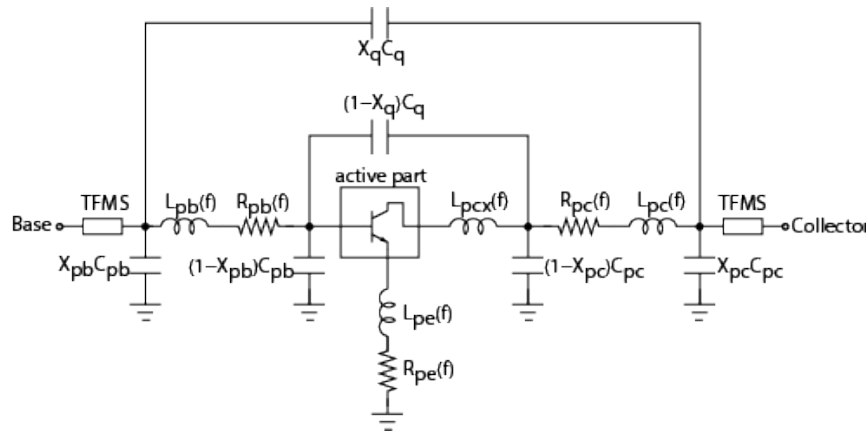
4-port EM simulation setup  
using GGB pico-probes or  
Cascade infinity probes –  
internal ports at transistor  
terminals



reference model



# EM-Simulation Assisted Extraction Procedure for InP HBT Small-Signal Reference Model Extraction<sup>1</sup>



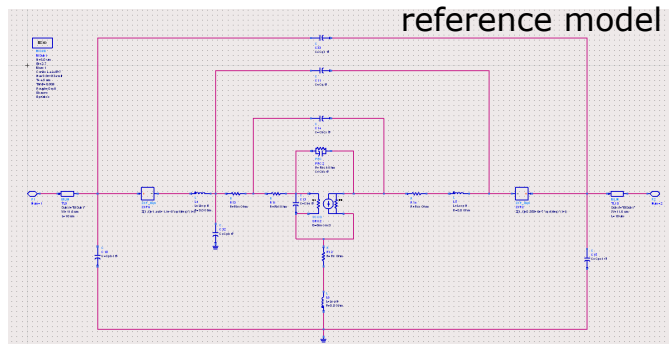
- The reference planes for model extraction are set by **multi-line Through-Reflect-Line (TRL) calibration** procedure using **on-wafer standards**
- The **extrinsic parasitic network** representing device electrodes and via transistions can be extracted from **3D EM-simulations** of the **passive device structure**
- The intrinsic model representing the **active device** can be extracted using **low-frequency S-parameters** only

**Table 1.** Parasitic model parameters (elements in parenthesis are extracted from cut-off mode measurements)

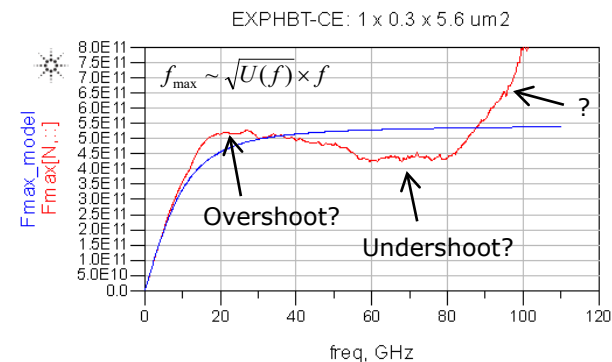
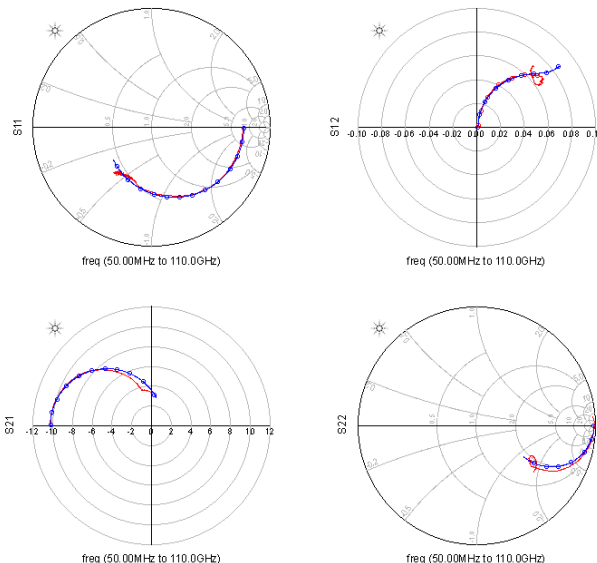
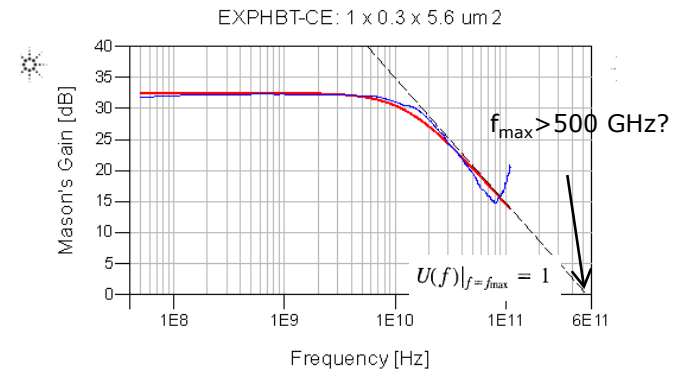
$C_{pb}$ [fF]	$X_{pb}$	$C_q$ [fF]	$X_q$	$C_{pc}$ [fF]	$X_{pc}$
4.6 (5.6)	0.36	1.3	0.15	2.0 (1.7)	1.0
$L_{pb}(f \rightarrow \infty)$ [pH]	$R_{pb}(f=0)$ [ $\Omega$ ]	$R_{pb,oc}$ [ $\Omega/\sqrt{\text{Hz}}$ ]	$L_{pcx}(f \rightarrow \infty)$ [pH]	$R_{pc}(f=0)$ [ $\Omega$ ]	$R_{pc,oc}$ [ $\Omega/\sqrt{\text{Hz}}$ ]
2.2	1.45	1.1E-6	0.3	0.0	0.0
$L_{pc}(f \rightarrow \infty)$ [pH]	$R_{pc}(f=0)$ [ $\Omega$ ]	$R_{pc,oc}$ [ $\Omega/\sqrt{\text{Hz}}$ ]	$L_{pcx}(f \rightarrow \infty)$ [pH]	$L_{TFMS}$ [ $\mu\text{m}$ ]	$W_{TFMS}$ [ $\mu\text{m}$ ]
0.0	0.35	6.0E-7	1.7	10.0	11.6

<sup>1</sup>T. K. Johansen et al., EM Simulation Assisted Parameter Extraction for Transferred-Substrate InP HBT Modeling, Int. Jour. Microwave and Wireless Tech., May 2018.

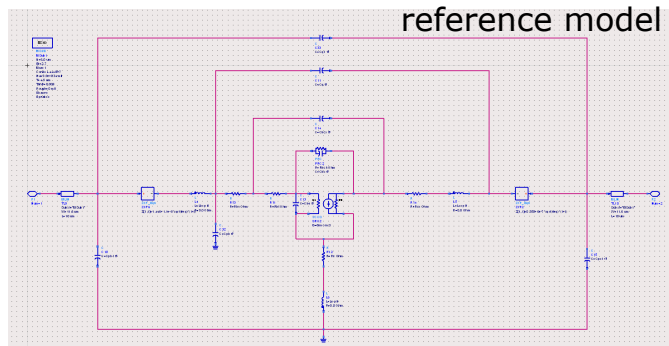
# Reference Model Compared to mTRL Calibrated Data using GGB Pico-Probes



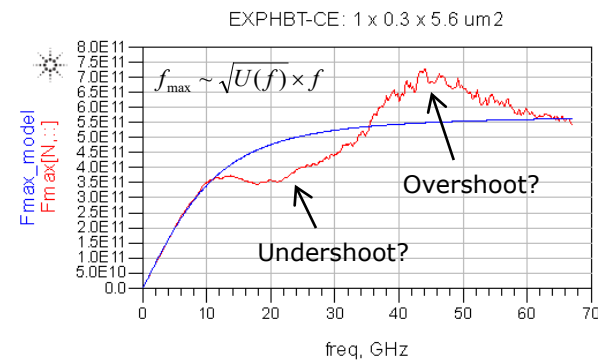
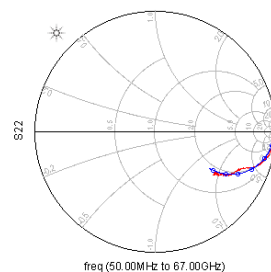
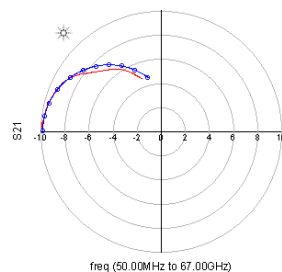
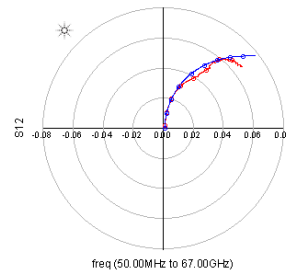
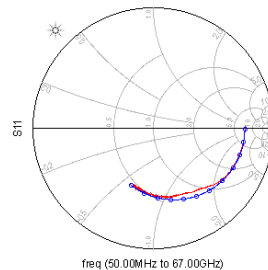
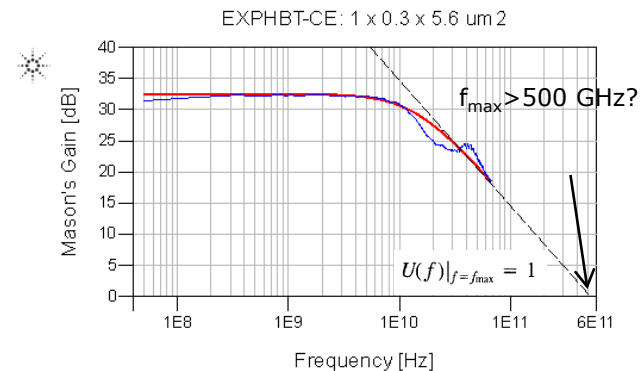
ENG3-X07 Small-Signal Modeling  
(EXPHBT-CE 1x0.3x6  $\mu\text{m}^2$  (type B1):  $V_{ce}=1.3\text{V}$ ,  $I_c=8.9\text{mA}$ )



# Reference Model Compared to mTRL Calibrated Data using Cascade Infinity Probes

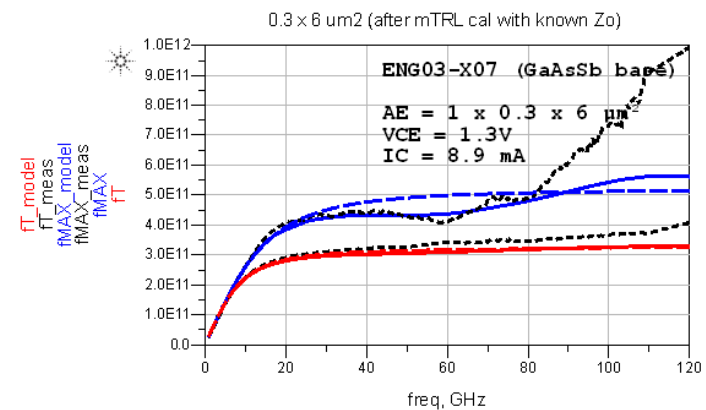
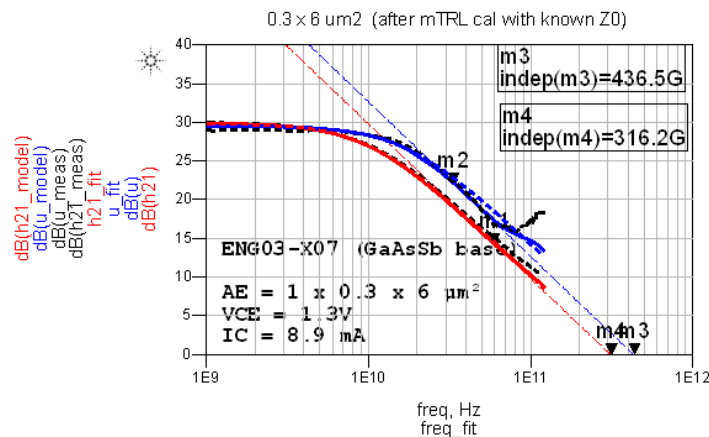


ENG3-X07 Small-Signal Modeling  
(EXPHBT-CE 1x0.3x6 um<sup>2</sup> (type B1): V<sub>ce</sub>=1.3V, I<sub>c</sub>=8.3mA)



# GGB Pico-probes Without Neighbour Coupling: Ceramic Carrier + Open Boundary

mTRL calibration procedure using CST simulated (MS150), MS420, MS1250, MS1950, MS2850, MS8500, Thru, Short, Open and Load



Solid lines (blue): mTRL corrected model –  $\text{dB}(U)$

Solid lines (red): mTRL corrected model -  $\text{dB}(h_{21})$

Dotted lines (black): mTRL corrected measurements

Dashed lines (blue): model reference –  $\text{dB}(U)$

Dashed lines (red): model reference -  $\text{dB}(h_{21})$

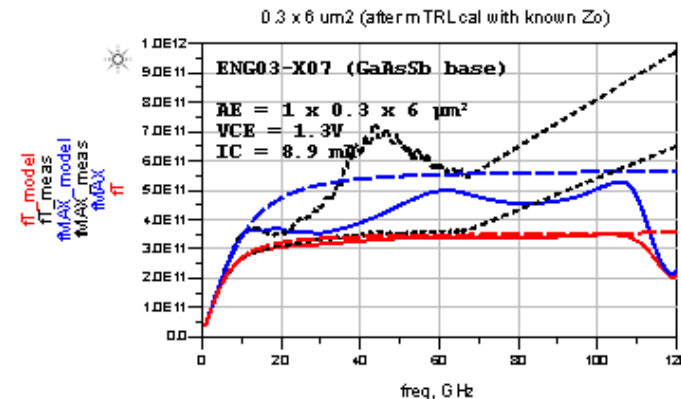
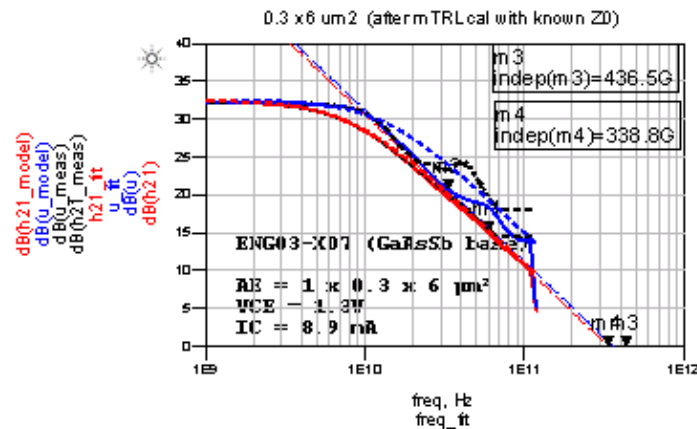
MASON's gain up to 80 GHz well predicted!

Strong increase above 80 GHz not predicted (neighbour coupling?). Measurements are only valid up to 110 GHz.



# Cascade Infinity Probes Without Neighbour Coupling: Ceramic Carrier + Open Boundary

mTRL calibration procedure using CST simulated (MS150), MS420, MS1250, MS1950, MS2850, MS8500, Thru, Short, Open and Load



Solid lines (blue): mTRL corrected model – dB(U)  
Solid lines (red): mTRL corrected model - dB(h<sub>21</sub>)  
Dotted lines (black): mTRL corrected measurements  
Dashed lines (blue): model reference – dB(U)  
Dashed lines (red): model reference - dB(h<sub>21</sub>)

Initial drop in MASON's gain around 15 - 20 GHz predicted! Overshoot frequency upshifted and of too low amplitude (neighbour coupling?). Measurements are only valid up to 67 GHz.

# Summary

- Characterization and modeling issues for downscaled sub-mm-wave InP DHBT devices related to the on-wafer measurement environment has been investigated:
- A full 3D EM simulation approach is proposed to analyze the effect of the on-wafer measurement environment on the characteristics of the downscaled sub-mm-wave InP DHBT devices, in particular Mason's gain
- While the results obtained using GGB pico-probes in connection with multi-line TRL on-wafer calibration can be reasonable well predicted **the reason** for the corruption has not yet been deeply analyzed
- The results obtained using Cascade infinity probes are well predicted in the lower frequency range but may require a more careful modeling of the on-wafer measurement environment

**Thank You**