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# Electromagnetic Modelling of Time-Variant Propagation Effects due to Rotating Wind Turbines

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# Overview

- Background: Influence of Wind Turbines on Operation of Air Surveillance Radar Systems
- Introduction: Measurement Campaigns
  - Ground Measurements
  - Commercial Hexacopter
- Electromagnetic Simulations of Wind Farm Scenarios
  - Ray Tracing Approach
  - Setup of Scenarios
  - Typical Results (Frequency Domain)
- Evaluation of Simulation Data in Time Domain
- Summary and Conclusions

# Measurement Equipment



Ground measurements

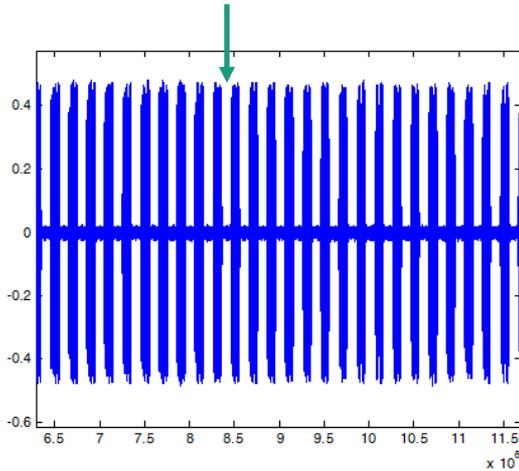


FHR experimental airplane „Delphin“



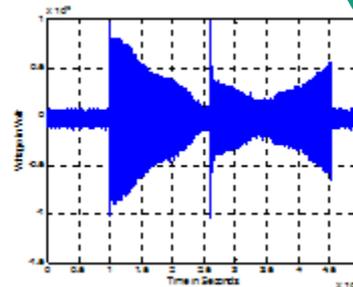
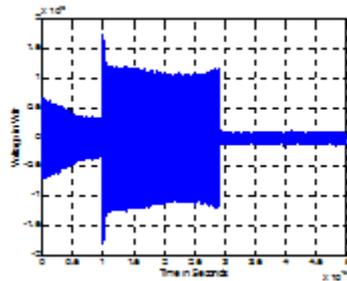
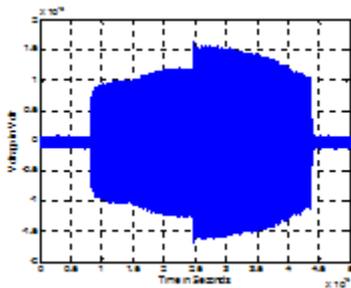
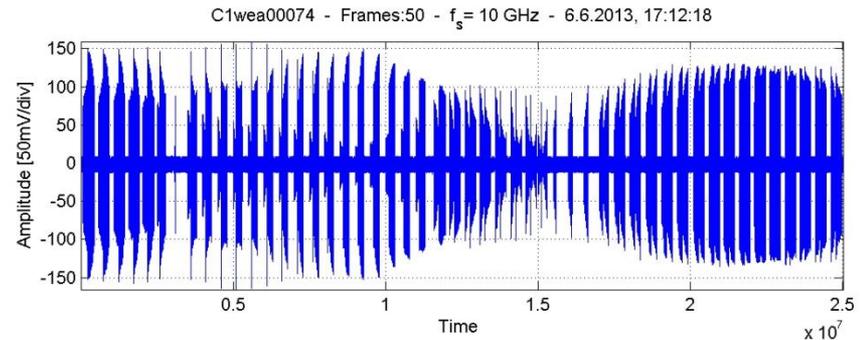
# Typical Measurement Results

Without WEA in propagation path:  
- Typical pulse series obtained



## Typical Observations behind WEAs:

- Fluctuations of pulse power over time
- Change of pulse modulation caused by WEA
- Effects observed in different measurements



With WEA in propagation path:

- Typical pulse series
- Typical pulse modulations

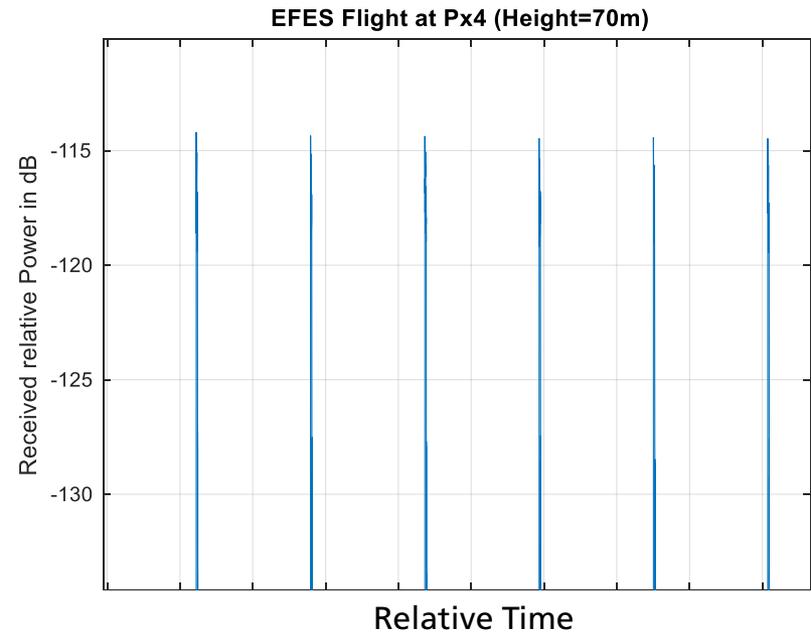
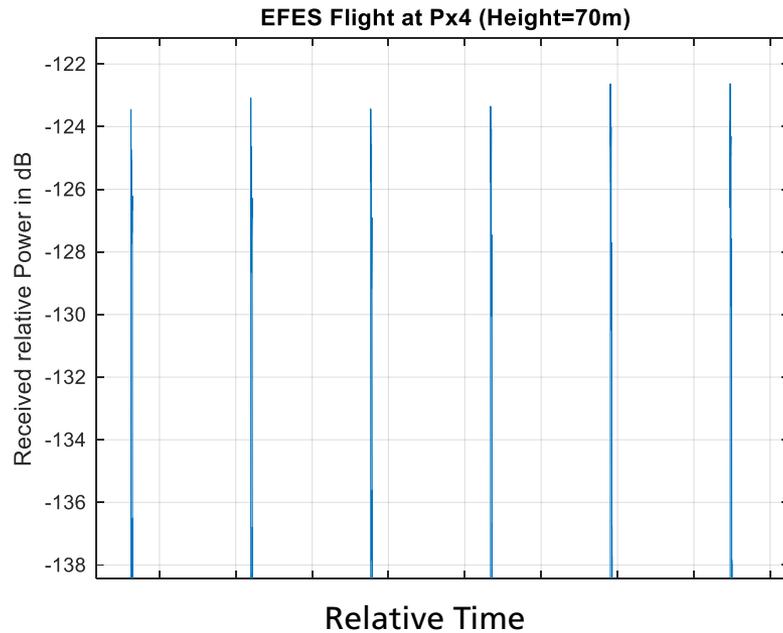
# Measurements Using a Hexacopter

## Measurement Platform:

- Commercially available hexacopter
- Control unit and receiver system designed for the measurements
- Field strengths at several locations have been recorded at different heights (max. 100 m)
- Antenna turned towards the air surveillance radar automatically
- Constant position during recording of field strength data
- Each data set covers a time frame including several pulses transmitted by the radar (corresponding to a very short cut through the simulated data)



# Measurement Results (1)



## Results at 70m height:

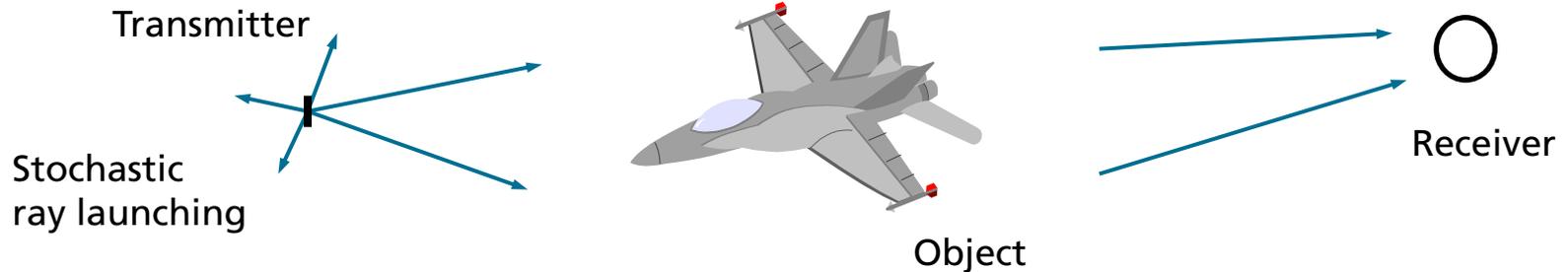
- Same height but during two different measurement sequences (corresponding to different rotation angles)
- Relative difference of 8 dB
- Good agreement of field strength variation with simulated data

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# Simulation Approach

## EM Fields Calculation with SBR Ray Tracing



### Ray Tracing Method:

*(Geometrical Calculation of Propagation Paths)*

Shooting-and-Bouncing Rays (SBR), number of reflections practically unlimited

Discrete rays as representatives of ray tubes

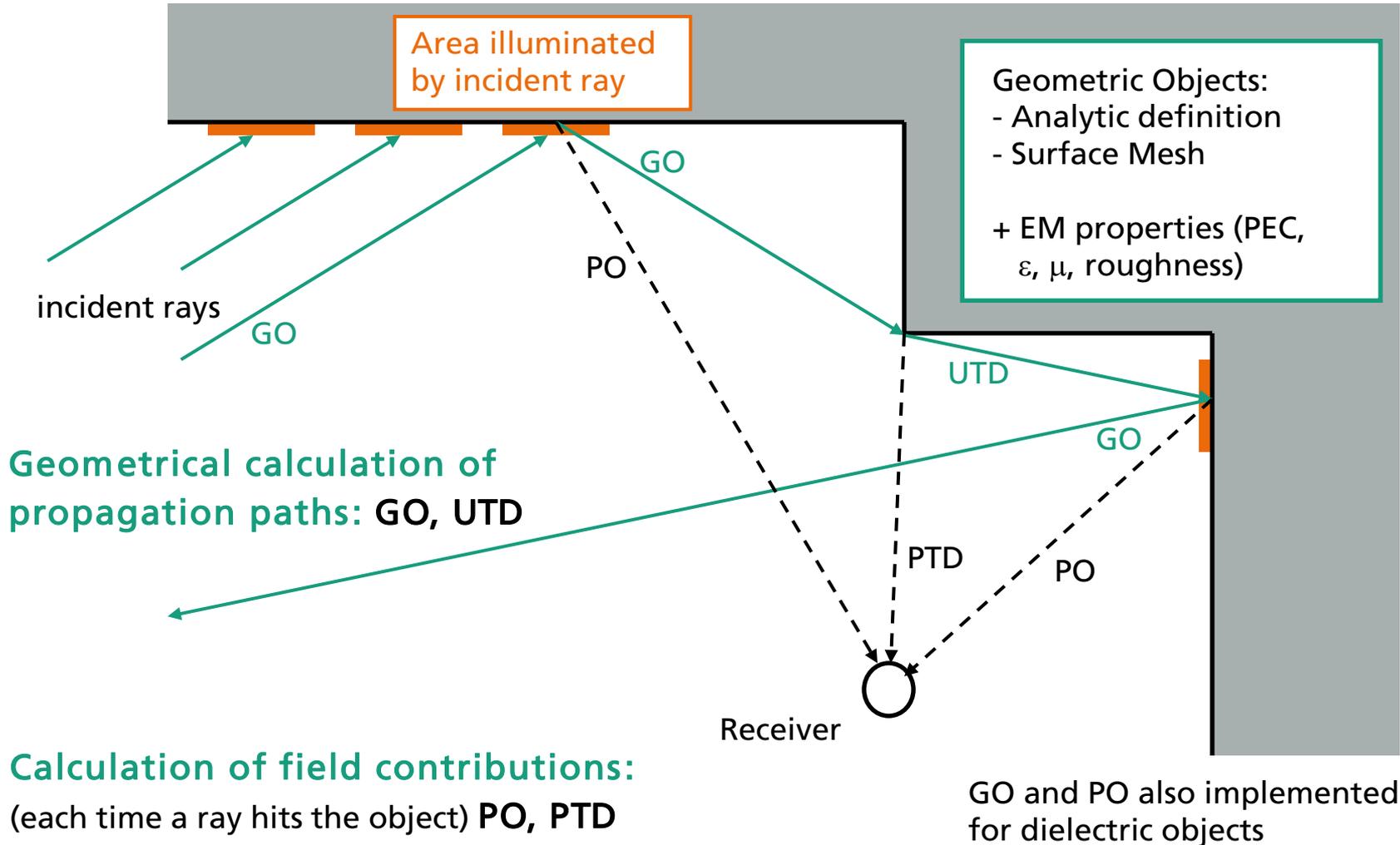
Ray-Density Normalisation (RDN) states the "distance" between rays

### Calculation of Field Strength Contributions to Receiver:

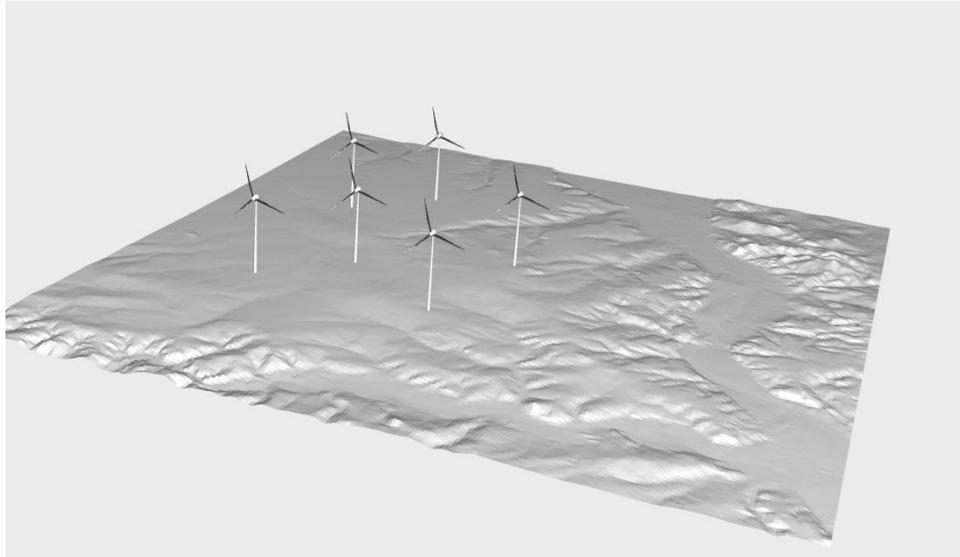
*(each time a ray hits the object)*

Physical Optics (PO) + Physical Theory of Diffraction (PTD)

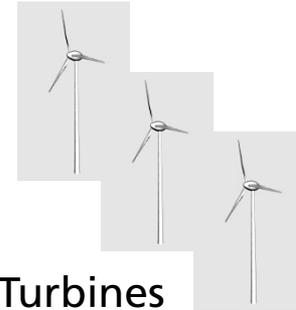
# Ray Tracing: Combination of GO/UTD-PO/PTD



# Schematic Setup of Simulations



Terrain (CAD-Model in NASTRAN format)



Wind Turbines  
(CAD-Model in NASTRAN format)

Transmitter Specification  
(Location, main lobe direction)

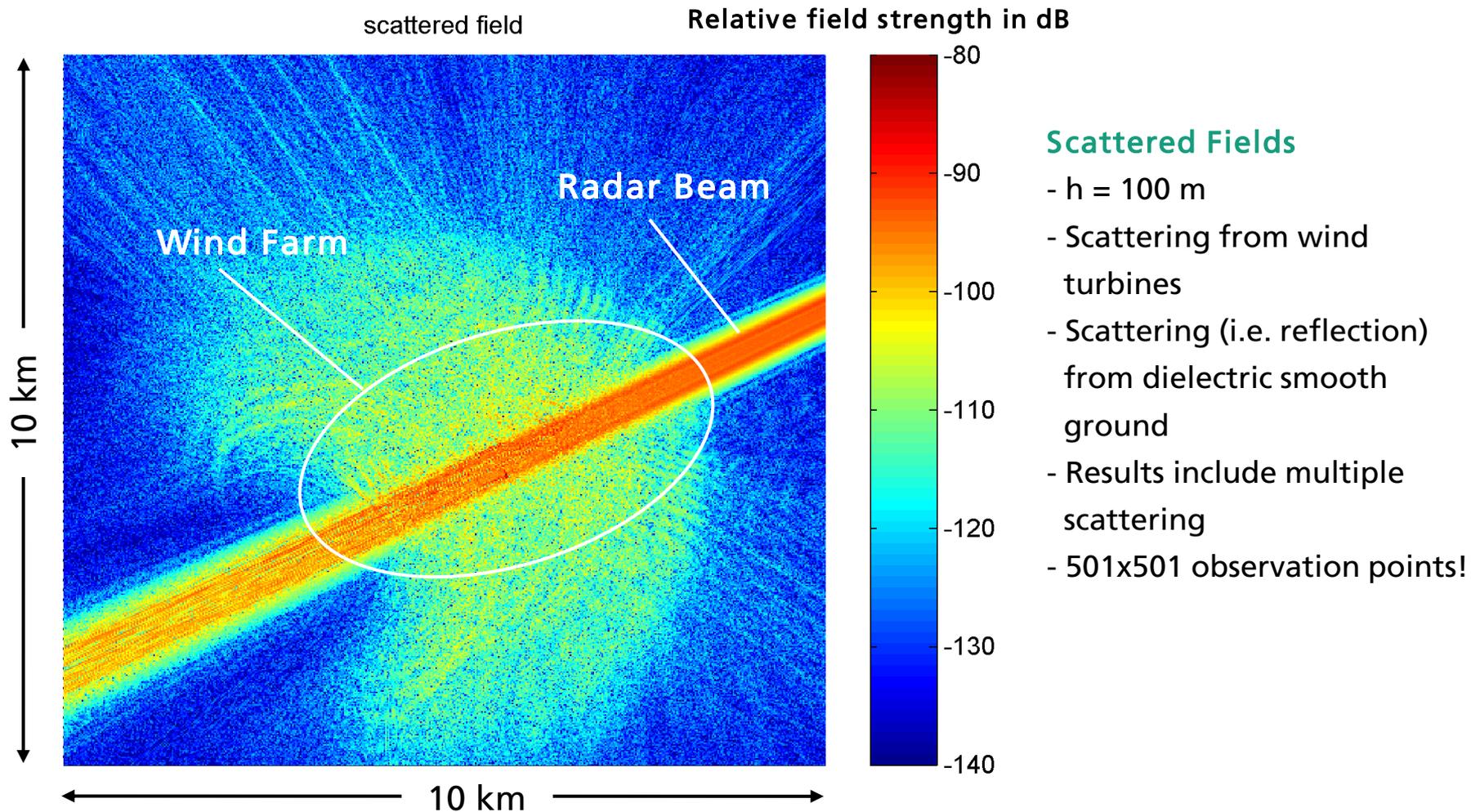
Receiver Specification  
(Single point, 1D, 2D arrays,...)



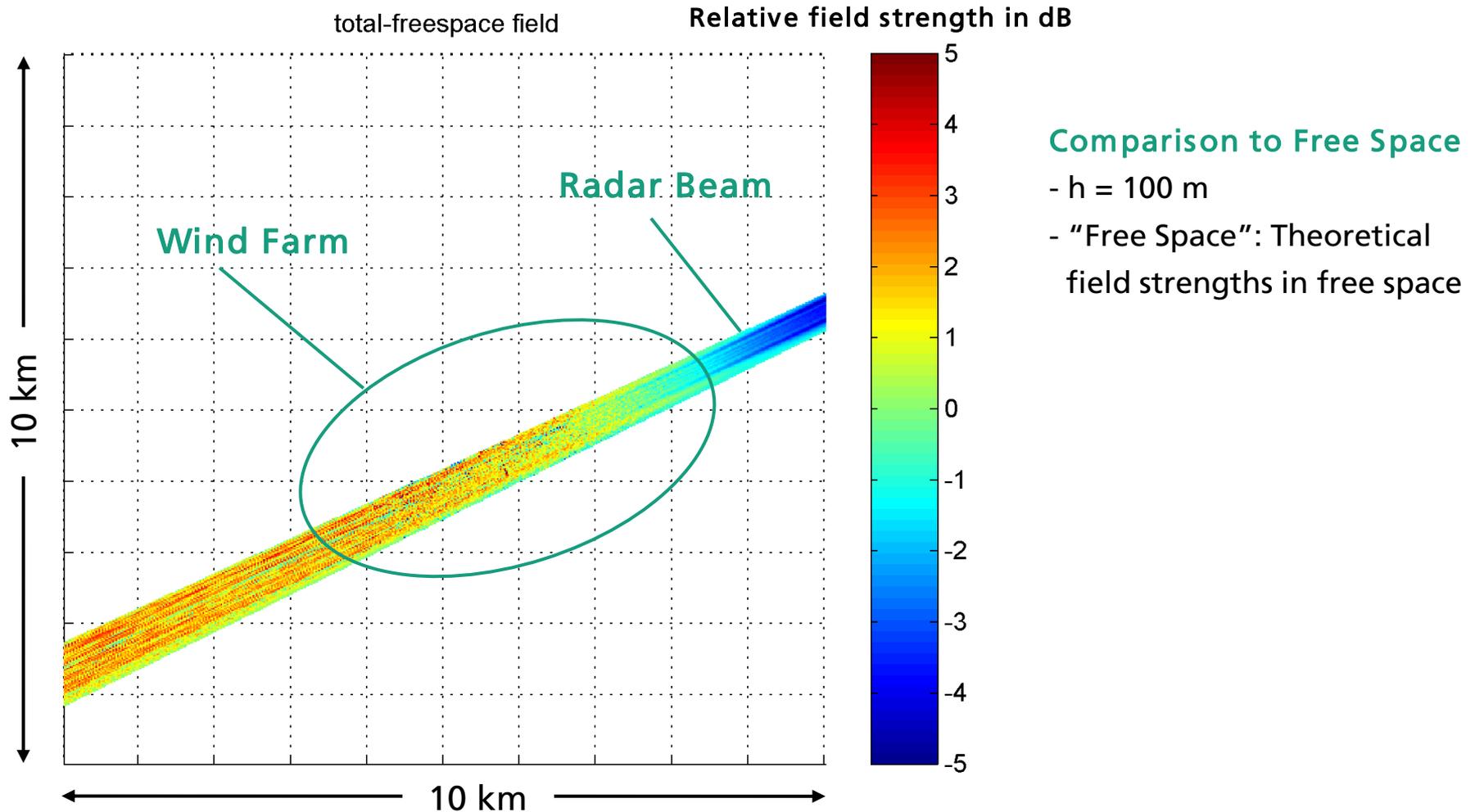
Ray Tracing Simulation

Output / Postprocessing:  
Field Strengths  
(Single point, 1D, 2D arrays,...)

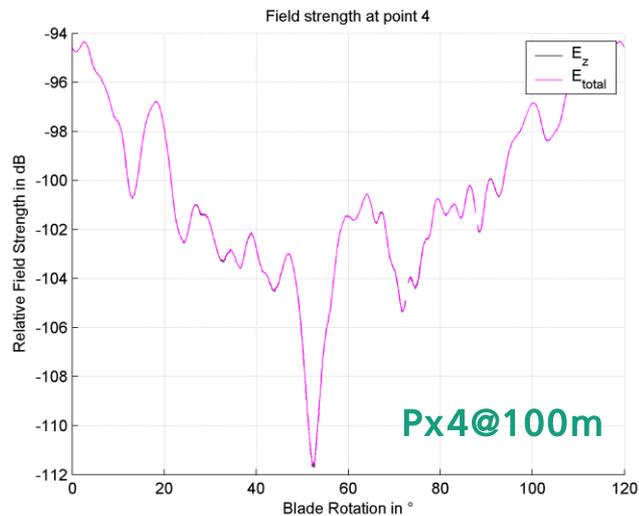
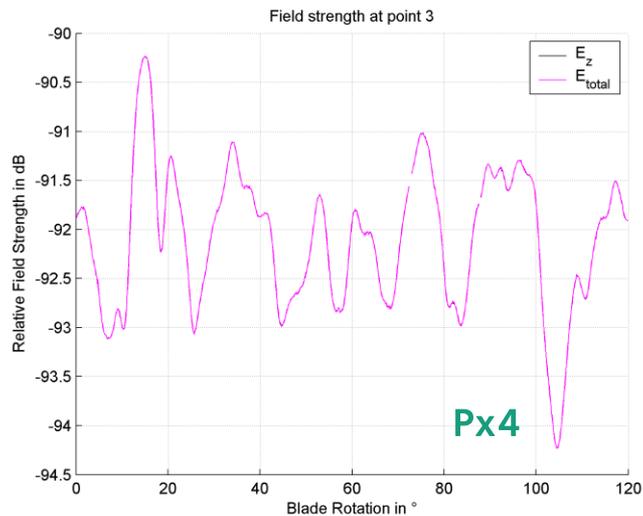
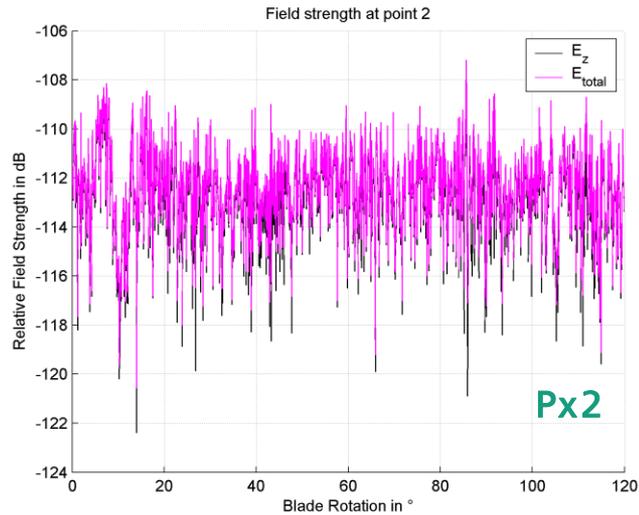
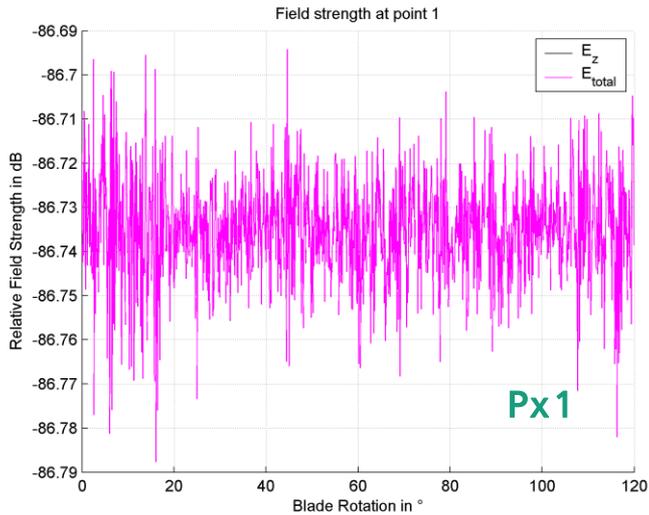
# Wind Farm, Static Scenario (2D Field Distribution)



# Simulation Results for Wind Farm (2D Field Distribution)



# Wind Farm, Rotating Blades



## Simulation Setup:

- Fixed observation points; sequence of quasi-static scenarios

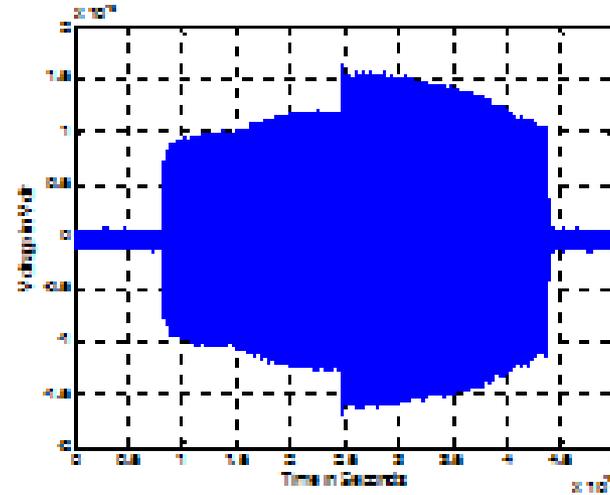
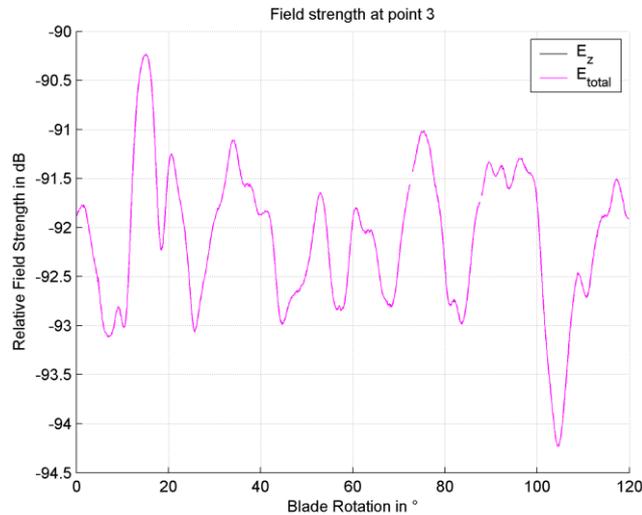
## Observation:

- Simulation data show variation of field strengths, similar behavior as in measurements
- Variation of field strength also for distant (50km, 100km) observation points

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# How to Compare Simulated and Measured Data



## Simulated Data:

- Approach 1: Sequence of data in **frequency domain**

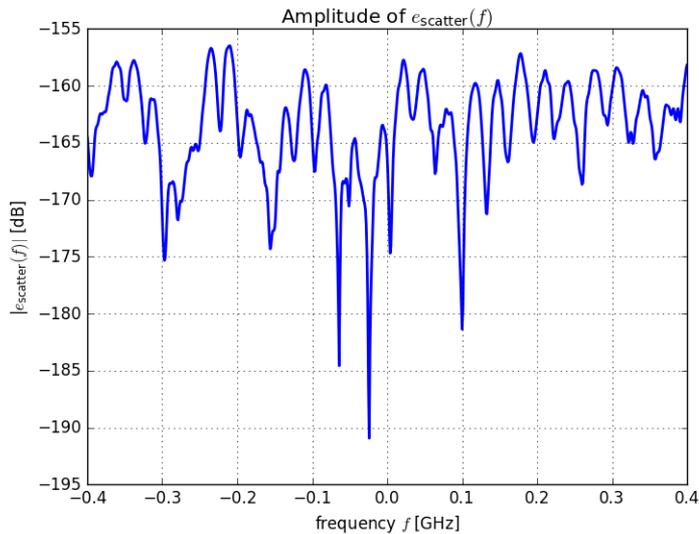
## Measured Data:

- Pulse modulation in **time domain**



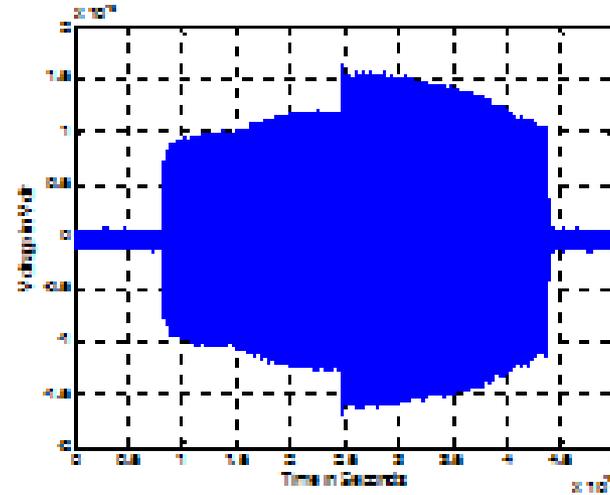
Results not exactly comparable

# How to Compare Simulated and Measured Data



## Simulated Data:

- Approach 2:  $N$  frequency data points
- Bandwidth:  $(N-1) \Delta f$
- covered time window:  $T = (N-1) \Delta t$ , should be large enough to contain the scattered pulse, which leads to a minimum number of frequency data points



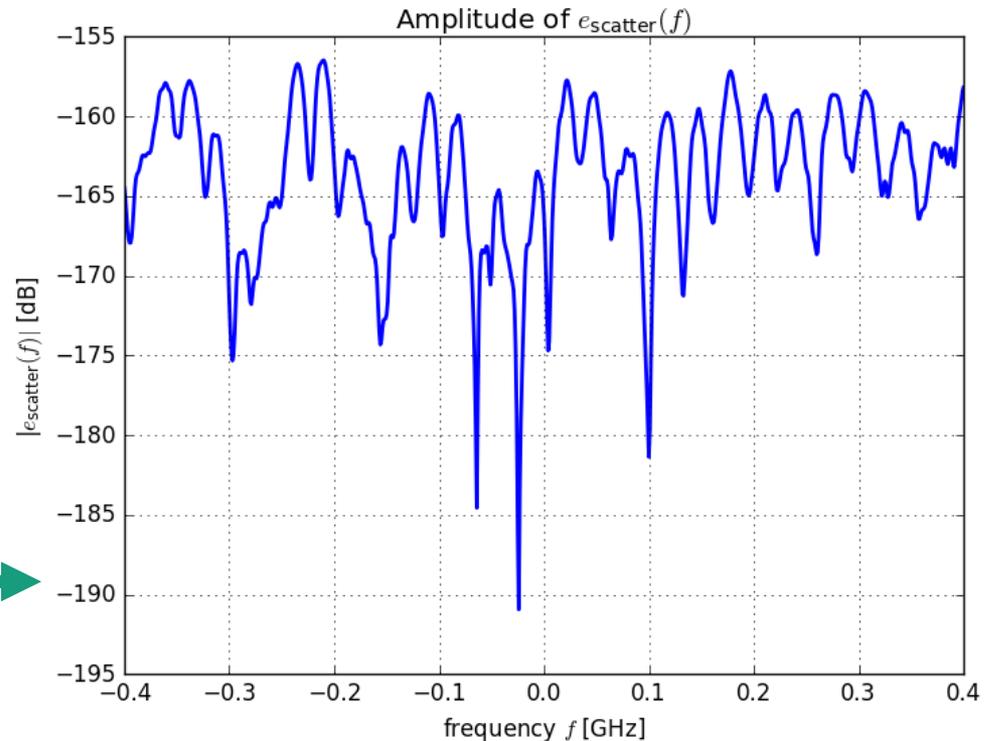
## Measured Data:

- Pulse modulation in **time domain**

# Simulation of Scattered Fields in Frequency Domain



Ray Tracing Simulation



## Simulation Data:

- Frequency Domain Method (GO+PO)
- Can be provided for a given bandwidth
- $e_{\text{scatter}}(f)$  is significantly frequency-dependent, as one would expect due to the superposition of scattering contributions from an electrically large structure

$$e_{\text{scatter},\text{sim}}(f) = \frac{E_{\text{scatter},\text{sim}}(f)}{E_{\text{init},\text{sim}}}$$

# Representation of Pulse Forms in Time Domain

## Arbitrary Electromagnetic Pulse

can be described as real part of:

$$\mathbf{E}(t) = [\mathbf{e}_v A_v(t) + \mathbf{e}_h A_h(t)] e^{j2\pi f_0 t}$$

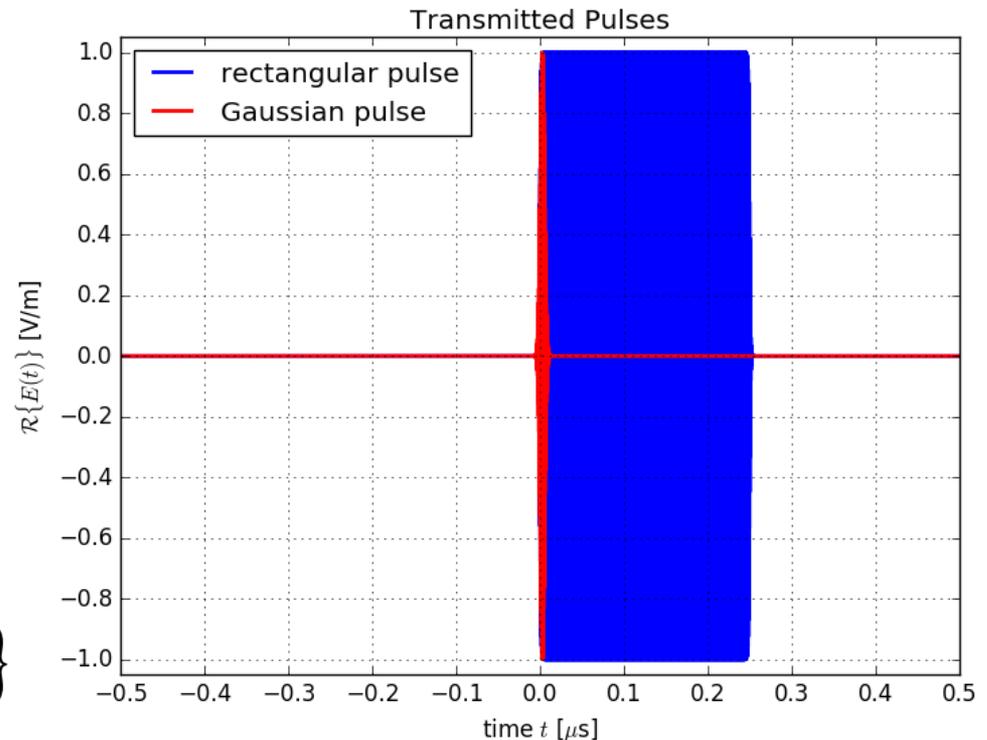
$A_i(t)$  [V/m] is the complex, time dependent envelope of the pulse

## Gaussian Pulse:

$$A_{\text{gauss}}(t) = A_0 e^{-\frac{(t-t_{\text{pulse}})^2}{2\sigma_{\text{gauss}}^2}}$$

## Smoothed Rectangular Pulse:

$$A_{\text{rect}}(t) = A_0 \left\{ \frac{1}{2} \left[ 1 + \tanh \left( \frac{t-t_{\text{rise}}}{T_{\text{rise}}} \right) \right] - \frac{1}{2} \left[ 1 + \tanh \left( \frac{t-t_{\text{fall}}}{T_{\text{fall}}} \right) \right] \right\}$$



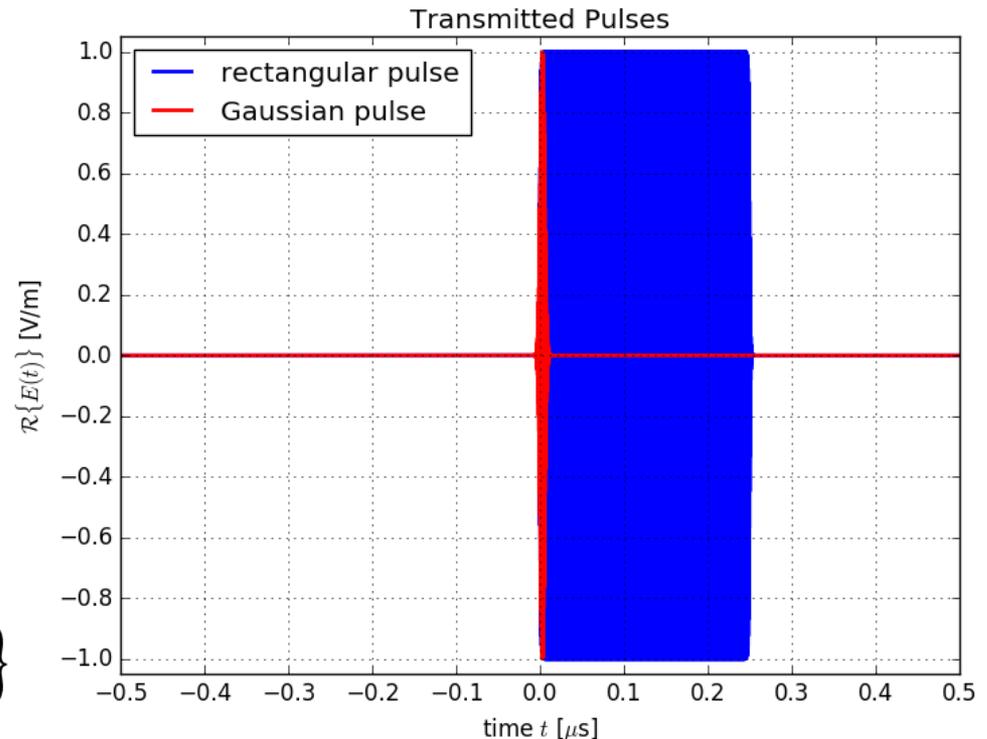
# Representation of Pulse Forms in Time Domain

## Gaussian Pulse:

$$A_{\text{gauss}}(t) = A_0 e^{-\frac{(t-t_{\text{pulse}})^2}{2\sigma_{\text{gauss}}^2}}$$

## Smoothed Rectangular Pulse:

$$A_{\text{rect}}(t) = A_0 \left\{ \frac{1}{2} \left[ 1 + \tanh \left( \frac{t-t_{\text{rise}}}{T_{\text{rise}}} \right) \right] - \frac{1}{2} \left[ 1 + \tanh \left( \frac{t-t_{\text{fall}}}{T_{\text{fall}}} \right) \right] \right\}$$



## Arbitrary choice of parameters (to showcase pertinent effects):

$T_{\text{rise}} = 1.25 \mu\text{s}$ , pulse duration: 2.5 ns (Gauss pulse), 0.25  $\mu\text{s}$  (rectangular pulse)

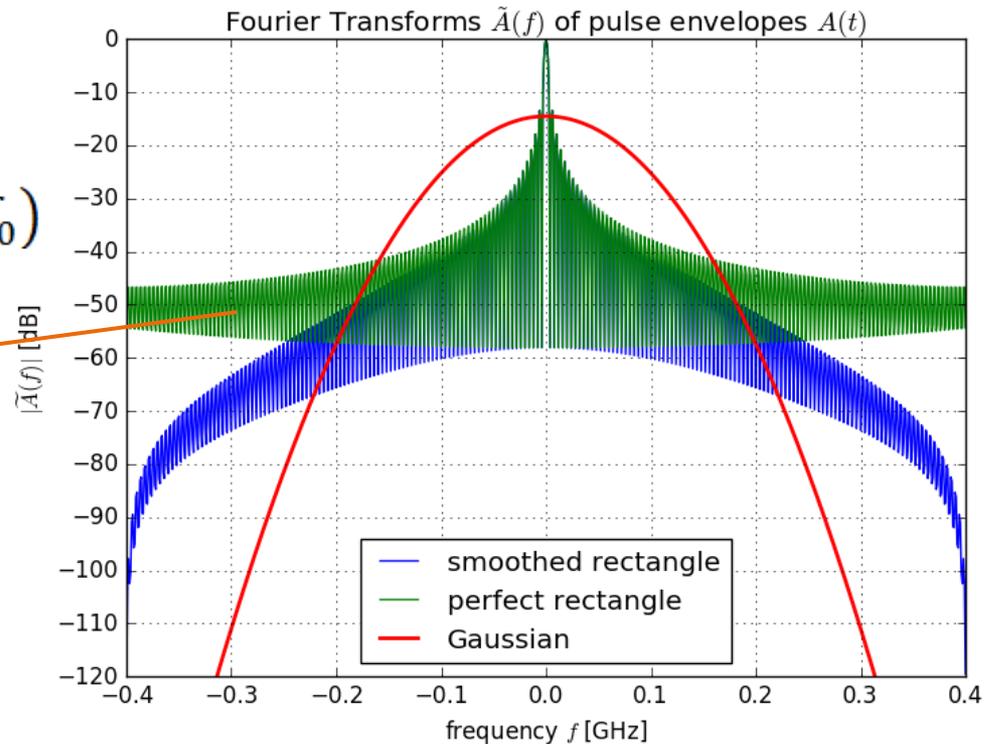
Bandwidth 0.8 GHz,  $\Delta f = 1$  MHz,  $T = 1 \mu\text{s}$

# Transformation of Pulses to Frequency Domain

## Fourier Transform of Electric Field:

$$F\{E(t)\} = \tilde{A}(f) * \delta(f-f_0) = \tilde{A}(f-f_0)$$

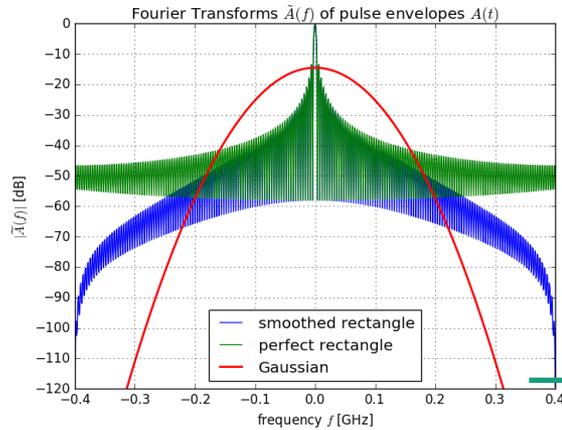
Perfect rectangular pulse for comparison



## After Fourier Transformation:

- Cut spectrum according to bandwidth of simulated data
- Might lead to inaccuracy if pulse has significant contributions out of simulated band

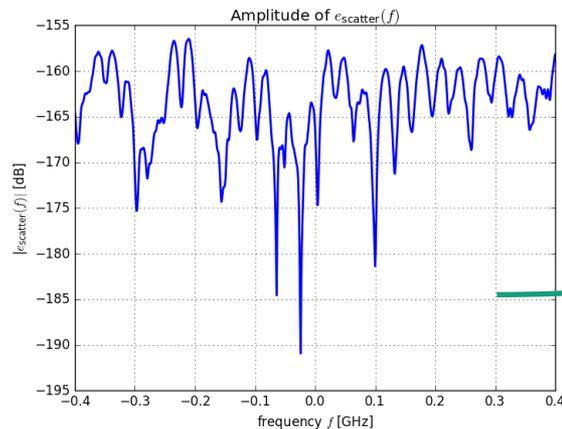
# Transformation back to Time Domain (1)



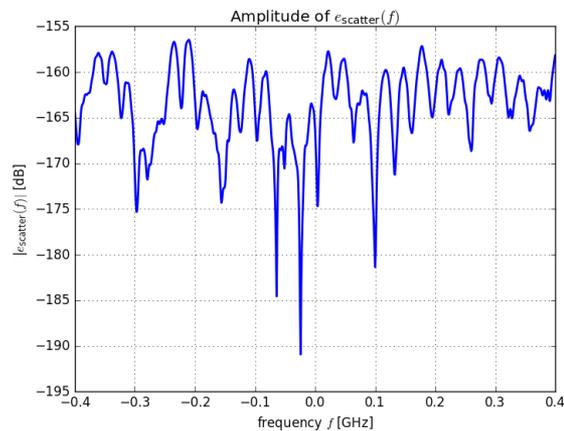
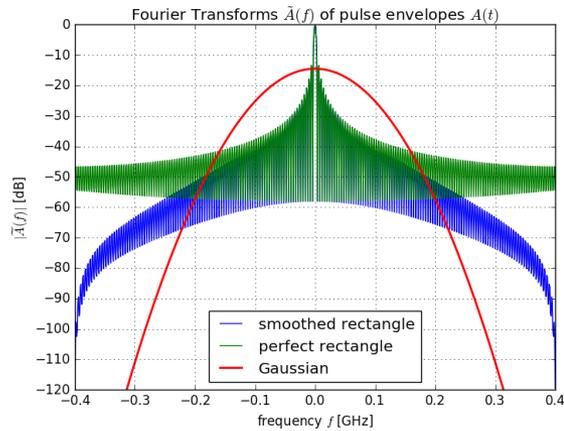
In frequency domain, the Fourier Transform of the pulse envelope is multiplied with the down-converted scattering results from the ray tracing simulation

Scattered Pulse in Time Domain:

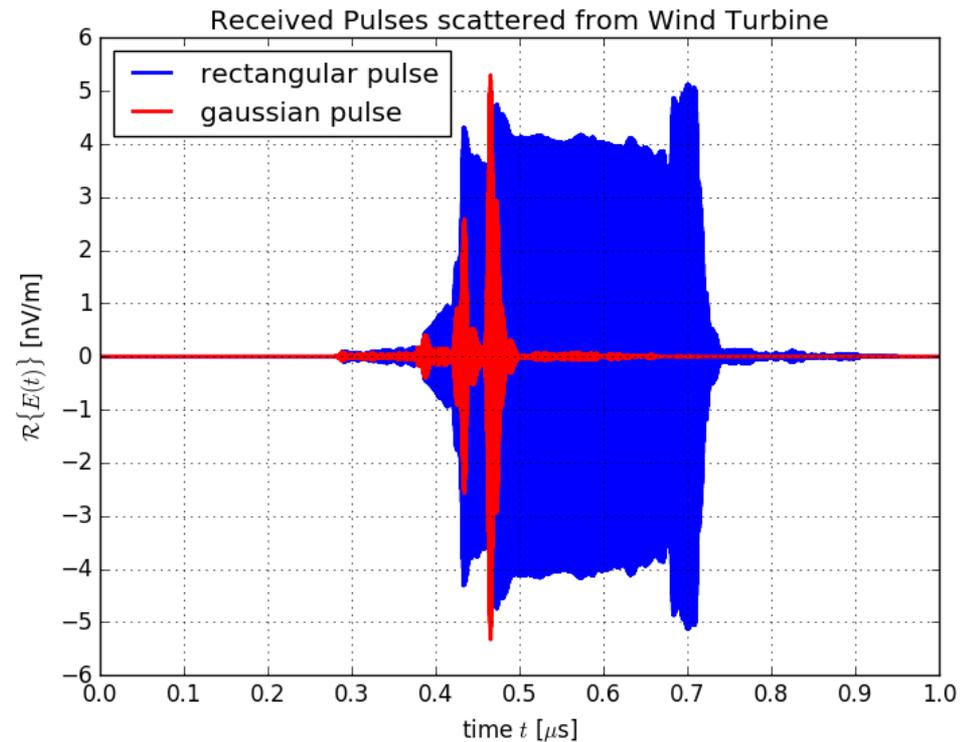
$$E_{\text{scatter}}(t) = F^{-1}\{e_{\text{scatter,sim}}(f + f_0)\tilde{A}(f) * \delta(f - f_0)\}$$
$$= F^{-1}\{e_{\text{scatter,sim}}(f + f_0)\tilde{A}(f)\}e^{j2\pi f_0 t}$$



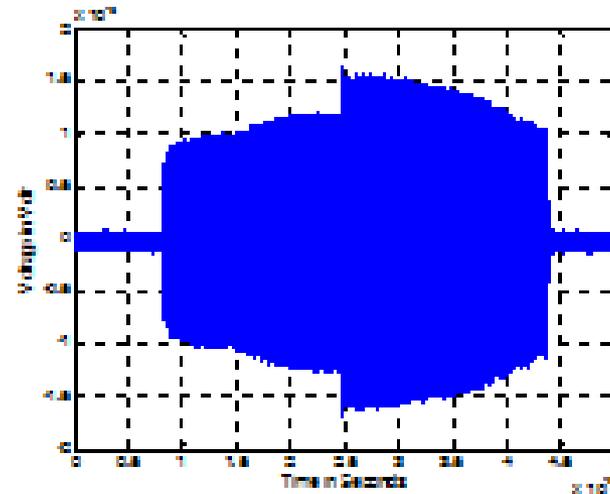
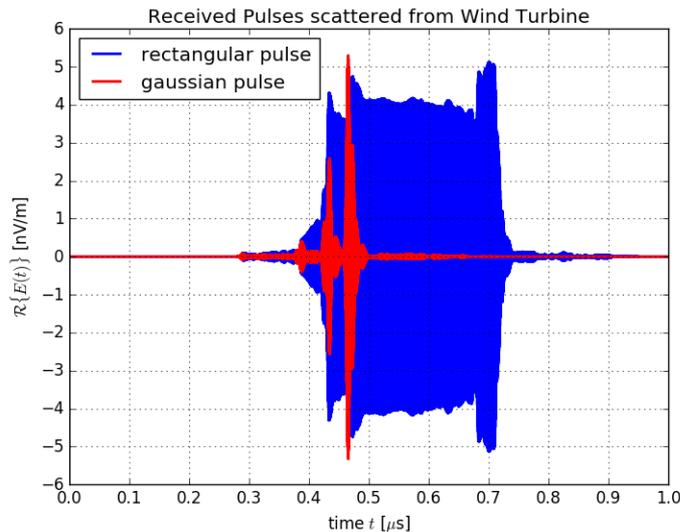
# Transformation back to Time Domain (2)



## Scattered Pulse in Time Domain:



# How to Compare Simulated and Measured Data (2)



## Simulated Data:

- Scattered pulse in **time domain**
- Time domain post-processing can be done for arbitrary pulses without the need of repeating the simulation for each pulse

## Measured Data:

- Pulse modulation in **time domain**

# Summary

- Measurements:  
Fluctuations in the order of several dB are to be expected for the electromagnetic fields behind wind farms
- EM Simulations:  
Frequency Domain Simulations; Studies of Time Variance:  
Good qualitative agreement with measurements
- Modelling of Scattered Pulses in Time Domain  
Broadband frequency domain simulation of scattered fields  
Multiplication with Fourier Transform of pulse  
Transformation back to time domain  
Time domain post-processing for arbitrary pulses

# Literature

- F. Weinmann, J. G. Worms, P. Knott, "The Influence of Time-Variant Propagation Effects due to Rotating Wind Turbines," 2017 European Radar Conference (EuRAD), 9-13 October 2017, Nuremberg, Germany.
- F. Weinmann, "EM Modelling of Radar Signatures of Targets Behind Wind Farms – A Time-Gating Ray Tracing Approach," 2016 European Radar Conference (EuRAD), 3-7 October 2016, London, UK.
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- F. Weinmann, J. G. Worms, "Time-Variant Scattering Properties of Wind Turbines," EuCAP 2015 9th European Conference on Antennas and Propagation, 13-17 April 2015, Lisbon, Portugal.
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- F. Weinmann, "Accurate Prediction of EM Scattering by Wind Turbines," EuCAP 2014 8th European Conference on Antennas and Propagation, 6-11 April 2014, The Hague, The Netherlands.