

# An advancement of the gravimetric isotope mixture method rendering the knowledge of the spike purity superfluous

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# An advancement of the gravimetric isotope mixture method rendering the knowledge of the spike purity superfluous

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#### Abstract

The gravimetric isotope mixture method is the primary method to determine absolute isotope ratios. This method, however, depends on the existence of suitable spike materials and knowledge of their purities. Determining the purity of the spikes can be tedious and labour-intensive. In this publication, an advancement of the gravimetric isotope mixture method, rendering the determination of the purity of the spike materials unnecessary, is presented. The advancement combines mass spectrometry and ion chromatography leading to an approach being independent of the purity of the spike materials. In the manuscript the mathematical background and the basic idea of the novel approach are described using a two-isotope system like copper or lithium.

 ${\bf Keywords:} \ {\rm Isotope \ amount \ ratios, \ Metrology, \ Mass \ spectrometry, \ Ion \ chromatography$ 

## 1 Introduction

Isotope amount ratios R are useful tools in many scientific areas, ranging from archaeology [1] to zoology [2]. Mass spectrometry is usually the method of choice for

the isotope analysis of samples. With mass spectrometry excellent precision can be obtained, but isotope amount ratios (unit mol mol<sup>-1</sup>) are not directly available. Users obtain ion intensity ratios r (unit V/V, A/A or s<sup>-1</sup>/s<sup>-1</sup>), which are numerically different from the isotope amount ratios, in some cases the difference is up to 25 % [3–6]. This difference is due to the so-called instrumental isotopic fractionation (IIF) [7] or mass bias. The second term is rather colloquial and does not describe the chemical and physical causes adequately. Both terms are collective terms for all possible effects which lead to the difference between the isotope amount ratio and the ion intensity ratio, for example different ionization probabilities, space charge effects or detection efficiencies. These effects can be minimized, but not totally eliminated, and therefore correction is needed, see equation 1.

$$R_i = \frac{n_i}{n_1} = K_i r_i = K_i \frac{I_i}{I_1} \tag{1}$$

 $R_i$  is the *i*<sup>th</sup> isotope ratio,  $n_i$  is the amount of substance of the *i*<sup>th</sup> isotope,  $n_1$  is the amount of substance of the so-called reference isotope, in most cases the most abundant isotope of the element under investigation.  $r_i$  is the ratio of the measured ion intensities of the  $i^{\text{th}}$  isotope and the reference isotope.  $I_i$  and  $I_1$  are the measured ion intensities of the *i*th isotope and the reference isotope, respectively.  $K_i$  is the so-called K-factor, which transforms the measured intensity ratio r into the isotope amount ratio R or in other words corrects for the mass bias. The K-factor can be determined by using a certified isotope reference material, which is to the International System of Units traceable (SI) and chemically as close as possible to the sample. The sample and reference need to be measured within the same campaign, since the IIF varies over time. With the knowledge of the certified isotope amount ratio and the measured ion intensity ratio of the reference material the K-factor can be determined by applying equation 1. This K-factor can also be used for the correction of the measured ion intensity ratio of the sample. This simple correction scheme requires that a suitable reference material exists. Since absolute isotope amount ratios are not directly available via mass spectrometry, the question arises how the isotopic composition of the reference material can be determined in the first place. This situation is quite similar to the famous chicken or the egg causality dilemma. Without knowing R, K cannot be determined and vice versa – a classical catch-22 situation. But there is a way out of this dilemma and it is known as the gravimetric isotope mixtures (GIM) method [8]. The GIM procedure is a primary method for the determination of SI-traceable isotope ratios. Since it is a primary method no prior knowledge of the true isotope ratio is required. Only measured quantities (not having the unit  $mol mol^{-1}$ ) are needed. In brief, the basic idea to derive the K-factors for a system with  $N_{\rm iso}$  isotopes is to have  $N_{\rm iso}$  spike materials (each enriched in one of the isotopes) and to prepare at least  $N_{\rm iso} - 1$  binary blends of these spike (or parent) materials under gravimetric control. In the following steps the ion intensity ratios of the parent materials and the binary blends are measured. The isotope amount ratios of the blends can be expressed as a function of the isotope amount fractions of the corresponding parent materials. These functions form a system of linear equations, which can be solved for the wanted

*K*-factors. More detailed information about the basic idea and the underlying mathematics can be found in the literature [9-12]. In case of a two-isotope system (e.g., lithium or copper) the *K*-factor can be expressed as [13, 14]:

$$K_{2} = \frac{M_{1}}{M_{2}} \frac{w_{\rm A} m_{\rm AB} \left( r_{\rm A,2} - r_{\rm AB,2} \right) + w_{\rm B} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} \right)}{w_{\rm A} m_{\rm AB} \left( r_{\rm AB,2} - r_{\rm A,2} \right) r_{\rm B,2} + w_{\rm B} m_{\rm BA} \left( r_{\rm AB,2} - r_{\rm B,2} \right) r_{\rm A,2}}$$
(2)

 $M_1$  is the atomic weight of the reference isotope (in the case of lithium <sup>7</sup>Li),  $M_2$  is the atomic weight of the other isotope. The small r's are the measured ion intensity ratios of the two parent materials (A and B) and the blend AB.  $m_{AB}$  and  $m_{BA}$  are the masses of the parent materials A and B, respectively, used for the preparation of the blend AB.  $w_A$  and  $w_B$  are the mass fractions of the element of interest in the parent materials, or in other words the purity of the parent materials. Since  $w_A$ and  $w_{\rm B}$  are needed, these have to be determined as well to derive the K-factor and finally the absolute isotope ratio R. The established primary method to determine the analyte content w is the so-called isotope dilution mass spectrometry (IDMS). The basic principles of the IDMS have been reviewed by Heumann [15] and Vogl et. al [16] and the underlying mathematics have been generalized by Ouerdane et al. [17]. Besides the fact, that the IDMS is both highly precise and accurate, it has several other advantages. For instance, once the sample has been well mixed with the spike material, loss of the mixture does not alter the result since only ratios (being intensive quantities) are measured. Another advantage is that it is less time consuming than standard addition [18]. For the determination of the analyte content, a reference material Z is needed, with a known content  $w_Z$ . Material Z is mixed with the sample/spike to be analysed (in this case A or B) and finally the isotope ratios in the parent materials and the blends are measured. Following the aforementioned procedure, the analyte content w of material A and material B can be expressed as:

$$w_{\rm A} = w_{\rm Z} \frac{m_{\rm ZA}}{m_{\rm AZ}} \frac{r_{\rm Z,2} - r_{\rm AZ,2}}{r_{\rm AZ,2} - r_{\rm A,2}} \frac{M_1 + K_2 r_{\rm A,2} M_2}{M_1 + K_2 r_{\rm Z,2} M_2} \tag{3}$$

and

$$w_{\rm B} = w_{\rm Z} \frac{m_{\rm ZB}}{m_{\rm BZ}} \frac{r_{\rm Z,2} - r_{\rm BZ,2}}{r_{\rm BZ,2} - r_{\rm B,2}} \frac{M_1 + K_2 r_{\rm B,2} M_2}{M_1 + K_2 r_{\rm Z,2} M_2}.$$
(4)

The three equations (2 to 4) form a system of non-linear equations. Although there are as many equations as unknowns (three equations and the three unknowns K,  $w_A$  and  $w_B$ ), there is no solution with a physical meaning. Solving this system leads to solutions where either  $w_A$  or  $w_B$  are zero and K is negative. The solutions are given in the supplement of this manuscript. A possible explanation could be that there is not enough information to describe the system mathematically correctly. While there are primary methods to determine absolute isotope ratios and the analyte content (GIM and IDMS) they cannot be combined to one method. Such a method would allow the determination of both quantities, due to the lack of additional mathematical information. Hence, it seems that it is impossible to determine absolute isotope amount ratios, without knowing the purity of the spike materials. A potential, but only theoretical, solution would be to have a second material Z2, with a known content. Instead of blend BZ blend BZ2 is prepared and equation 4 changes accordingly. Since there are now

three truly independent equations a unique solution can be found. But this approach has no practical meaning, since two conditions must be fulfilled. Firstly, there must be a second material Z2, which is hardly the case and secondly, the isotopic composition of Z2 must be significantly different from Z. If the latter condition is not fulfilled the correct K-factor can be calculated but the relative uncertainty associated with it increases dramatically the more similar the isotopic composition of Z and Z2 are. In the supplement, a simulation showing the described effect can be found as well as the algebraic solutions. This publication moreover presents a possible solution to this issue. Since the method is based on the GIM method and additional ion chromatography measurements, it is called ICeGIM, which is short for Ion Chromatography enhanced Gravimetric Isotope Mixtures.

### 2 Basic Idea and Mathematical Derivation

In this section a solution to the problem described above is presented. The solution is an advancement of the GIM method. The basic idea of the advancement is schematically depicted for a two-isotope system in figure 1, and will be explained step-by-step. In theory the method presented can be used for systems with two or more isotopes, but for the sake of simplicity only a two-isotope system is considered here. The aim of the following mathematical considerations is to eliminate  $w_A$  and  $w_B$  from equation 2. The isotope amount ratio  $R_{AB}$  of the blend AB can be expressed as:

$$R_{AB,2} = \frac{n_2}{n_1} = \frac{x_{A,2}n_A + x_{B,2}n_B}{x_{A,1}n_A + x_{B,1}n_B}(,)$$
(5)

where  $n_{\rm A}$  and  $n_{\rm B}$  are the amounts of substance of the materials A and B used for the preparation of blend AB.  $x_{{\rm A},i}$  is the amount-of-substance fraction of the  $i^{\rm th}$ isotope in material A, and  $x_{{\rm B},i}$  is analogously defined. Next the substance content  $\beta$ is introduced,  $\beta$  is defined as<sup>1</sup>:

$$\beta_i = \frac{n_i}{m_i},\tag{6}$$

where  $m_i$  is the mass of the respective solution. This mass includes impurities, solvents etc., and  $n_i$  is the amount of substance of the analyte.

Every  $x_i$  can be expressed as

$$x_i = \frac{R_i}{\sum_{j=1}^{N_{\rm iso}} R_j}.\tag{7}$$

With  $R_i = K_i r_i$ , equation 5 can be reformulated as:

$$K_2 r_{AB,2} = \frac{\beta_A m_{AB} \frac{K_2 r_{A,2}}{1 + K_2 r_{A,2}} + \beta_B m_{BA} \frac{K_2 r_{B,2}}{1 + K_2 r_{B,2}}}{\beta_A m_{AB} \frac{1}{1 + K_2 r_{A,2}} + \beta_B m_{BA} \frac{1}{1 + K_2 r_{B,2}}}$$
(8)

Equation 8 can be solved for K.

<sup>&</sup>lt;sup>1</sup>The International Union of Pure and Applied Chemistry (IUPAC) does not recommend a single symbol for the substance content but n/m [19]. In this publication the symbol  $\beta$  is used for the sake of briefness.

<sup>7</sup> 

$$K_{2} = \frac{\beta_{\rm A} m_{\rm AB} \left( r_{\rm A,2} - r_{\rm AB,2} \right) + \beta_{\rm B} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} \right)}{\beta_{\rm A} m_{\rm AB} \left( r_{\rm B,2} - r_{\rm B,2} - r_{\rm B,2} r_{\rm A,2} \right) + \beta_{\rm B} m_{\rm BA} \left( r_{\rm A,2} r_{\rm AB,2} - r_{\rm A,2} r_{\rm B,2} \right)} \tag{9}$$

Now an expression for  $\beta_i$  must be found since  $n_i$  is unknown, and the isotopic composition of material *i* is also not known.  $\beta_i$  can also be expressed as:

$$\beta_i = \frac{n_i}{m_i} \frac{\frac{M_i}{m_i}}{\frac{M_i}{m_i}} = \frac{w_i}{M_i} \tag{10}$$

By considering equation 7, the molar mass  $M_i$  can be expressed as:

$$M_i = \frac{1}{1+R_i}M_1 + \frac{R_i}{1+R_i}M_2 \tag{11}$$

Combining equations 10 and 11 and considering  $R_i = K_i r_i$  in the case of the reference material Z, leads to:

$$\beta_{\rm Z} = \frac{w_{\rm Z}}{\frac{1}{1+R_{\rm Z,2}}M_1 + \frac{R_{\rm Z,2}}{1+R_{\rm Z,2}}M_2} = \frac{w_{\rm Z}}{\frac{1}{1+R_{\rm Z,2}}(M_1 + R_{\rm Z,2}M_2)}$$

$$= \frac{w_{\rm Z}\left(1+R_{\rm Z,2}\right)}{M_1 + R_{\rm Z,2}M_2} = \frac{w_{\rm Z}\left(1+K_2r_{\rm Z,2}\right)}{M_1 + K_2r_{\rm Z,2}M_2}$$
(12)

Now a way has to be found to express  $\beta_A$  and  $\beta_B$  in terms of  $\beta_Z$ , since only  $w_Z$  is known. Here, ion chromatography (IC) might be a useful tool. The area A under the peak in the chromatogram is proportional to the ratio of the amount of substance of the corresponding ion to the mass of the loaded analyte mass. For this approach another material Y is needed. Material Y is an internal standard, which does not contain the element of the other materials A, B and Z. In the next step three blends are prepared under gravimetric control; ZY, AY and BY, see figure 1 lower part. For instance blend ZY is prepared by mixing mass  $m_{ZY}$  of material Z with mass  $m_{YZ}$  of material Y. AY and BY are prepared analogously. The area  $A_Z$  of the peak of the main element of Z in the blend ZY can mathematically be expressed as:

$$A_{\rm Z} = k_{\rm Z} \beta_{\rm Z} \frac{m_{\rm ZY}}{m_{\rm sln,Z}} \tag{13}$$

 $k_{\rm ZY}$  is the sensitivity coefficient. It depends on the specific ion (e.g. Li<sup>+</sup>), the conductivity detection, the ion exchange column and other parameters. k is however constant for a specific ion, as long as the samples have a similar chemical composition and the same set-up has been used for the measurement.  $m_{\rm ZY}$  is the mass of material Z used to prepare ZY and  $m_{\rm sln,Z}$  is the total mass of the solution including  $m_{\rm ZY}$ ,  $m_{\rm YZ}$  and  $m_{\rm dil}$  being the mass of the added solvent, if further dilution is necessary. For better clarification, the area  $A_{\rm Z}$  is depicted in the box called ZY in figure 1. It is shaded in two colours since it is a result of the two isotopes of the element of interest. In a similar way the area  $A_{\rm Y}$  (blue shaded in box ZY of figure 1) can be expressed as:

$$A_{\rm YZ} = k_{\rm YZ} \beta_{\rm Y} \frac{m_{\rm YZ}}{m_{\rm sln,Z}} \tag{14}$$

All quantities occurring in equation 14 are analogously defined to those in equation 13. The ratio  $f_Z$  of these two areas is:

$$f_{\rm Z} = \frac{A_{\rm Z}}{A_{\rm YZ}} = \frac{k_{\rm ZY}}{k_{\rm YZ}} \frac{\beta_{\rm Z}}{\beta_{\rm Y}} \frac{m_{\rm ZY}}{m_{\rm YZ}}$$
(15)

In the case of the two other blends (AY and BY) the ratio of the two peak areas can be expressed analogously.

$$f_X = \frac{A_X}{A_{YX}} = \frac{k_X}{k_{YX}} \frac{\beta_X}{\beta_Y} \frac{m_{XY}}{m_{YX}}, X \in \{A, B\}$$
(16)

Since the sensitivity coefficient k is constant for a specific ion, the following is valid.

$$\frac{k_{\rm A}}{k_{\rm YA}} = \frac{k_{\rm B}}{k_{\rm YB}} = \frac{k_{\rm Z}}{k_{\rm YZ}} \tag{17}$$

From equation 15 follows:

$$\frac{k_{\rm YZ}}{k_{\rm Z}} = \frac{1}{f_{\rm Z}} \frac{\beta_{\rm Z}}{\beta_{\rm Y}} \frac{m_{\rm ZY}}{m_{\rm YZ}} \tag{18}$$

Now combining equations 15 and 18 allows to express  $\beta_A$  and  $\beta_B$  as:

$$\beta_{\rm A} = w_{\rm Z} \frac{1 + K_2 r_{\rm Z,2}}{M_1 + K_2 r_{\rm Z,2} M_2} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{m_{\rm YA}}{m_{\rm AY}} \frac{f_{\rm A}}{f_{\rm Z}}$$
(19)

and

$$\beta_{\rm B} = w_{\rm Z} \frac{1 + K_2 r_{\rm Z,2}}{M_1 + K_2 r_{\rm Z,2} M_2} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}},\tag{20}$$

respectively. These two expressions (equations 19 and 20) can be inserted into equation 9, which then can be solved for K, leading to:

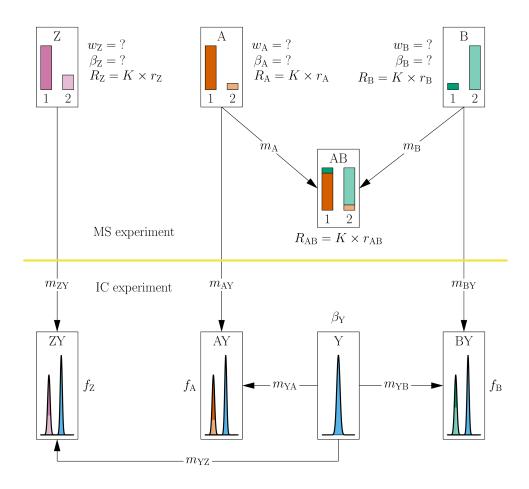
$$K_{2} = \frac{\frac{m_{\rm YA}}{m_{\rm AY}} f_{\rm A} m_{\rm AB} \left( r_{\rm A,2} - r_{\rm AB,2} \right) + \frac{m_{\rm YB}}{m_{\rm BY}} f_{\rm B} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} \right)}{\frac{m_{\rm YA}}{m_{\rm AY}} f_{\rm A} m_{\rm AB} \left( r_{\rm B,2} r_{\rm AB,2} - r_{\rm B,2} r_{\rm A,2} \right) + \frac{m_{\rm YB}}{m_{\rm BY}} f_{\rm B} m_{\rm BA} \left( r_{\rm A,2} r_{\rm AB,2} - r_{\rm A,2} r_{\rm B,2} \right)}$$
(21)

All steps leading to equation 21 are shown in the electronic supplement of this publication. With the knowledge of K also  $w_A$  and  $w_B$  can be calculated, by using equations 3 and 4. This applies, in the case that additional mixtures of Z + A and Z + B are prepared. At this point it should be added, that  $w_A$  and  $w_B$  can also be expressed only in terms of measured quantities (so without directly using K). But since these expressions are quite long they are only shown in the electronic supplement. In short: Equations 19 and 20 can be rearranged yielding:

$$w_{\rm A} = w_{\rm Z} \frac{1 + Kr_{\rm Z}}{1 + Kr_{\rm A}} \frac{M_1 + Kr_{\rm A}M_2}{M_1 + Kr_{\rm Z}M_2} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{m_{\rm YA}}{m_{\rm AY}} \frac{f_{\rm A}}{f_{\rm Z}}$$
(22)

and

$$w_{\rm B} = w_{\rm Z} \frac{1 + Kr_{\rm Z}}{1 + Kr_{\rm B}} \frac{M_1 + Kr_{\rm B}M_2}{M_1 + Kr_{\rm Z}M_2} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}}$$
(23)



**Fig. 1** Schematic presentation of the ICeGIM method. The upper part of the figure shows the mass spectrometry experiment including the measurement of the standard material Z, the two spike materials A and B and the blend AB. The masses  $m_{AB}$  and  $m_{BA}$  are the amounts of material A and material B used for the preparation of AB, respectively. The lower part shows the ion chromatography experiment. This includes measurements of three blends. These blends consist of the internal standard Y and of the materials A,B or Z. The masses  $(m_{YX} \text{ or } m_{XY} \text{ with } X \in \{A, B, Z\})$  are the amounts of the corresponding material used to prepare the three blends AY, BY and ZY. All unknown (or wanted) quantities are marked with a question mark.

Inserting equation 21 into the last two equations yields equations ?? and ?? in the supplement. From equation 21 it can easily be seen that ICeGIM allows determination of absolute isotope ratios without knowing the purity of the spike materials and that therefore their associated uncertainties do not contribute to the uncertainties of the absolute isotope ratios. This feature is especially useful if the spike material is not a high purity metal but a chemical compound with unknown stoichiometry and

molar mass (e.g.  $\text{Li}_2\text{CO}_3$ ). Actually, even knowledge of  $w_Z$  is not needed for the determination of absolute isotope ratios. Hence, material Z can be any material with a similar chemical composition, but it is an important feature of the ICeGIM method that if you are only interested in the isotope ratios alone, no material Z is needed (see eq. 21). Also the molar masses of the materials A and B ( $M_A$ ,  $M_B$ ) are not needed. Equation 2 shows another characteristic of ICeGIM. Unlike GIM, ICeGIM does not require knowledge of the atomic masses of the isotopes. This is due to the usage of ion chromatography, since here all isotopes are detected as one signal. Besides ion chromatography, other analytical techniques could also be used. These might be inductively coupled plasma atomic emission spectrometry, conductometry, quantitative nuclear magnetic resonance (qNMR) or any other method which delivers signals being proportional to the amount-of-substance fraction of the analyte irrespective of the isotopic composition.

#### **3** Simulation and Uncertainty Consideration

To test the advancement of the GIM method presented above, a simulation has been performed. The simulation can be found in the electronic supplement of this publication. The purpose of this simulation was to demonstrate the principal of ICeGIM and also to assess the achievable uncertainties. The supplement enables potential users to perform their own calculations using their own data. In this simulation copper was chosen as the possible two-isotope system. Real values and realistic estimates of the uncertainties associated with the input quantities were used to assess the achievable uncertainties. For example, in the simulation the NIST material 3114 [20] was used as the certified reference material Z. In table 1, the relative uncertainties used in this simulation are listed. These uncertainties are typical for each of the input quantities. Since ICeGIM depends on IC measurements the achievable precision of IC is crucial. Brennan et al. [21] showed that by applying internal standardization analyte anion mass fractions can be determined with expanded relative uncertainties as low as 0.2%. This value can be seen as upper limit, since the peak area ratio is only one part of the uncertainty budget reported by Brennan et al. Also Rökher et al. [22] reported similar relative uncertainties for Li, Na, K, Mg and Ca. Therefore, 0.1% is a reasonable but conservative estimate for the relative uncertainty associated with  $f_{\rm A}$  or  $f_{\rm B}$ . The whole data set can be found in the supplement part 2.

The calculation of the associated uncertainty of K was done by a Monte Carlo simulation following internationally accepted rules and recommendations [23–25]. The result obtained using 1 000 000 trials is shown in figure 2 and K = 0.9455(33) mol V/mol V, with k = 2, was determined. The relative expanded uncertainty  $U_{\rm rel}$  is 0.35 %, which is in the same order of magnitude if compared with previous two-isotope GIM experiments, such as Malinovsky et al. (carbon,  $U_{\rm rel} = 0.22 \%$ ) [26], or De Bièvre et al. (boron,  $U_{\rm rel} = 0.26 \%$ ) [27]. At this point it must be stressed, that such a comparison of different isotope systems can only be a general orientation. Nevertheless the simulation shows that with ICeGIM comparable uncertainties could be obtained. It should be added that correlation was not considered in the simulation. Therefore, it is likely that lower uncertainties can be achieved.

Table 1Relative uncertainty of allinput quantities used in thissimulation.

relative uncertainty	value in $\%$	
$u(f_{\rm A})$	0.10	
$u(f_{\rm B})$	0.10	
$u(m_{AB})$	0.022	
$u(m_{\rm BA})$	0.019	
$u(m_{\rm YA})$	0.028	
$u(m_{\rm AY})$	0.053	
$u(m_{\rm YB})$	0.029	
$u(m_{\rm BY})$	0.057	
$u(r_{\mathrm{A},2})$	0.010	
$u(r_{\mathrm{B},2})$	0.010	
$u(r_{\mathrm{AB},2})$	0.0010	

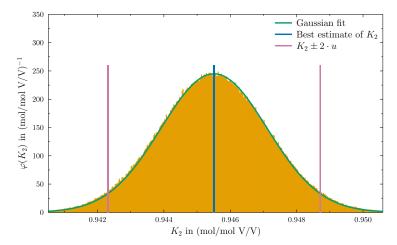


Fig. 2 Probability density of  $K_2$  derived using 10<sup>6</sup> Monte Carlo trials. The green curve represents the Gaussian fit, the two purple lines represent  $K_2 \pm 2 \cdot u$  and the blue line represents the best estimate of  $K_2$ .

## 4 Generalization

In the second section of this publication, the mathematics of the ICeGIM method have been derived for a two-isotope system. This approach can be generalized for systems with an arbitrary number of isotopes  $N_{\rm iso}$ . The above-described mathematical problem can be transformed into a matrix equation. The whole transformation is given in the supplement.

$$\mathbf{A}\,\mathbf{k} = \mathbf{b} \tag{24}$$

Matrix **A** is defined as:

$$\begin{aligned}
A_{i,j} &= \\ \begin{pmatrix} r_{AX(i+1),i+1} \cdot r_{A,j+1} - r_{X(i),i+1} \cdot r_{A,j+1} \end{pmatrix} \cdot m_{YX(i+1)} \cdot m_{AY} \cdot m_{X(i+1)A} \cdot f_{X(i+1)} - \\ \begin{pmatrix} r_{AX(i+1),i+1} \cdot r_{X(j),i+1} - r_{A,i+1} \cdot r_{X(j),i+1} \end{pmatrix} \cdot m_{X(i+1)Y} \cdot m_{YA} \cdot m_{AX(i+1)} \cdot f_{A} \end{aligned}$$
(25)

*i* and *j* are running variables (from 1 to  $N_{iso} - 1$ ), X(i) is a function returning the *i*<sup>th</sup> letter of the alphabet (e.g. X(2)=B), and all other quantities are analogously defined as in the above-mentioned two-isotope system.

The vector  $\mathbf{k}$  contains all the K-factors, therefore it is defined as:

$$k_i = K_{i+1}, i \in \{1, N_{\text{iso}} - 1\}$$
(26)

And finally, vector  $\mathbf{b}$  is defined as:

$$b_{i} = -\begin{bmatrix} \left( r_{AX(i),i} - r_{X(i),i+1} \right) \cdot m_{YX(i+1)} \cdot m_{AY} \cdot m_{X(i+1)Y} \cdot f_{X(i+1)} + \\ \left( r_{AX(i+1),i+1} - r_{A,i+1} \right) \cdot m_{X(i+1)Y} \cdot m_{YA} \cdot m_{AX(i+1)} \cdot f_{A} \end{bmatrix}$$
(27)

By multiplying equation 24 with  $\mathbf{A}^{-1}$  (the inverse of  $\mathbf{A}$ ), the wanted K-factors can be calculated. Note, inverting a matrix is computationally expensive and for larger systems it is advisable to use methods like Gaussian elimination, Cholesky decomposition or LU decomposition. The latter is implemented in the accompanying supplement to this paper. Applying Cramer's rule allows a generic solution for the K-factors to be formulated. It is noteworthy that Ouerdane et al. [17] also employed Cramer's rule to solve IDMS equations.

$$K_{i+1} = \frac{\det\left(\mathbf{A}_{i}\right)}{\det\left(\mathbf{A}\right)} \tag{28}$$

 $\mathbf{A}_i$  can be formed by replacing the  $i^{\text{th}}$  column with the vector **b**. The above equations allow the easy calculate the wanted K-factors for systems with an arbitrary number of isotopes and therefore also the uncertainties associated with them.

#### **5** Conclusion and Prospects

For the determination of absolute isotope ratios, knowledge of the purities of the spike materials used for the preparation of the gravimetric mixtures was needed. In this publication, an advancement of the primary method "gravimetric isotope mixtures" is presented. The method described above combines mass spectrometry and ion chromatography measurements. This approach has a distinct advantage over the classical GIM method. The purities of the spike materials are not needed any longer and therefore also do not contribute to the uncertainty of the absolute isotope ratios. This is a big advantage since ICeGIM allows to determine absolute isotope ratios in cases where no certified content reference material exists. This is a huge advantage especially in cases where no high purity metals are available but only salts with unknown stoichiometry and molar mass. In principle, the purities of the spike materials could be very low and do not have to be known with high accuracy. This is the case as long

as measurements are not biased by it. For example, if the matrices (impurities) of the spike materials are very different from the sample this would lead to quite different conditions in the argon plasma and, therefore leading to a different mass bias. The mathematical background of ICeGIM for a two-isotope system has been presented in detail. An initial simulation with realistic data demonstrated that, in terms of achievable uncertainties, ICeGIM is a reasonable alternative, when determining the spike purity is not possible. Moreover, it is worth further developing and testing this alternative method. In the last section the mathematical ansatz was generalized, so that the ICeGIM approach can be applied to any number of isotopes. First practical tests will be presented in a follow-up publication.

### 6 Declarations

Conflict of interest The authors declare no competing interests.

Author contribution statement Lukas Flierl: writing – original draft, conceptualization, visualization, simulation. Olaf Rienitz: witing – review & editing, conceptualization, visualization, supervision. Jochen Vogl: Writing – review & editing, Conceptualization. Axel Pramann: Writing – review & editing, Conceptualization. All authors read and approved the final manuscript.

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# Appendix: List of Quantities

Symbol	Unit	Quantity	Property
K	mol V/mol V	Mass bias correction factor	Result
$w_{\mathrm{A}}$	g/g	Mass fraction of analyte element in enriched parent solution A	Unknown
$w_{\rm B}$	g/g	Mass fraction of analyte element in enriched parent solution B	Unknown
$w_{\mathrm{Z}}$	g/g	Mass fraction of analyte element in natural standard solution Z	certified
$\beta_{\rm A}$	mol/g	Substance content of enriched analyte element in parent solution A with $bA = wA/MA$	Unknown
$\beta_{\rm B}$	$\mathrm{mol/g}$	Substance content of enriched analyte element in parent solution B with $bB = wB/MB$	Unknown
$R_i$	mol/mol	Amount ratio of spike isotope (2) over refer- ence isotope (1) in sample, standard, parent or mixture $i$ with $i \in \{A, B, Z, AB\}$ and $R = Kr$	Unknown
$r_i$	V/V	Signal intensity ratio of spike isotope (2) over reference isotope (1) in sample, standard, par- ent or mixture <i>i</i> with $i \in \{A, B, Z, AB\}$ and R = Kr	Measured (MS)
$m_{ m A}$	g	Mass of parent solution A blended with parent solution B to yield mixture AB	Measured (balance)
$m_{\rm B}$	g	Mass of parent solution B blended with parent solution A to yield mixture AB	Measured (balance)

 Table 2
 Quantities used in the GIM method. MS is short for mass spectrometry.

Symbol	Unit	Quantity	Property
$m_{\rm AY}$	g	Mass of parent solution A blended with inter- nal standard solution Y to yield mixture AY	Measured (balance)
$m_{\rm YA}$	g	Mass of internal standard solution Y blended with parent solution A to yield mixture AY	Measured (balance)
$m_{\rm BY}$	g	Mass of parent solution B blended with inter- nal standard solution Y to yield mixture BY	Measured (balance)
$m_{\rm YB}$	g	Mass of internal standard solution Y blended with parent solution B to yield mixture BY	Measured (balance)
$m_{\rm ZY}$	g	Mass of standard solution Z blended with internal standard solution Y to yield mixture ZY	Measured (balance)
$m_{\rm YZ}$	g	Mass of internal standard solution Y blended with standard solution Z to yield mixture ZY	Measured (balance)

**Table 3** Quantities (masses) used the in preparation of the blend needed for the IC measurements

Table 4Quantities obtained by IC.

Symbol	Unit	Quantity	Property
fA	μS/ <sub>min</sub>	Ratio of the area of the chromato- graphic peak of the analyte element over the area of the chromatographic peak of the internal standard element (ion chromatography) in the mixture AY of parent solution A and internal standard solution Y	Measured (IC)
$f_{ m B}$	μS/min	Ratio of the area of the chromato- graphic peak of the analyte element over the area of the chromatographic peak of the internal standard element (ion chromatography) in the mixture BY of parent solution B and internal standard solution Y	Measured (IC)
fz	μS/min	Ratio of the area of the chromato- graphic peak of the analyte element over the area of the chromatographic peak of the internal standard element (ion chromatography) in the mixture ZY of standard solution Z and internal standard solution Y	Measured (IC)

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## 7 Supplement

Supplement to "An advancement of the gravimetric isotope mixture method rendering the knowledge of the spike purity superfluous"

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## Preface

All equations occurring in this text are numbered as "S.X", equations labelled only with an integer number are the same as in the main part of this manuscript.

## 1 Non-physical Solutions of Equations 2, 3 and 4

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As mentioned in the main part of this publication, solving equations 2, 3 and 4 leads to solutions with no physical meaning. These solutions are:

$$K_{2} = \begin{cases} -\frac{M_{1}}{M_{2}r_{\text{A},2}} \\ -\frac{M_{1}}{M_{2}r_{\text{B},2}} \end{cases}$$
(S.1)

$$w_{\rm A} = \begin{cases} 0 \\ -w_{\rm Z} \frac{m_{\rm ZA}(r_{\rm A,2} - r_{\rm B,2})(r_{\rm AZ,2} - r_{\rm Z,2})}{m_{\rm AZ}(r_{\rm A,2} - r_{\rm AZ,2})(r_{\rm B,2} - r_{\rm Z,2})} \end{cases}$$
(S.2)

$$w_{\rm B} = \begin{cases} w_{\rm Z} \frac{m_{\rm ZB}(r_{\rm A,2} - r_{\rm B,2})(r_{\rm BZ,2} - r_{\rm Z,2})}{m_{\rm BZ}(r_{\rm A,2} - r_{\rm Z,2})(r_{\rm B,2} - r_{\rm BZ,2})} \\ 0 \end{cases}$$
(S.3)

### 2 IDMS with two Reference Materials

In the main manuscript, it was mentioned that the described problem could be solved by using a second reference material Z2. Instead of blend BZ, BZ2 is prepared, hence equation 4 becomes:

$$w_{\rm B} = w_{\rm Z2} \frac{m_{\rm Z2B,2}}{m_{\rm BZ2,2}} \frac{r_{\rm Z2,2} - r_{\rm BZ2,2}}{r_{\rm BZ2,2} - r_{\rm B,2}} \frac{M_1 + K_2 r_{\rm B,2} M_2}{M_1 + K r_{\rm Z2,2} M_2}.$$
 (S.4)

By considering equations 3, 2 and S.4 the  $K_2$ -factor can expressed as:

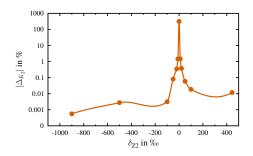
$$K_{2} = \frac{M_{1}(m_{AB}m_{BZ2}m_{AZ1}(r_{AB,2}-r_{A,2})(r_{Z1,2}-r_{AZ1,2})(r_{B,2}-r_{BZ2,2})w_{Z1} + m_{AZ1}m_{BA}m_{BZ2}(r_{AB,2}-r_{B,2})(r_{A,2}-r_{AZ1,2})(r_{Z2,2}-r_{BZ2,2})w_{Z2,2})}{M_{2}(m_{AB}m_{BZ2}m_{AZ1}r_{Z2,2}(r_{A,2}-r_{AB,2})(r_{Z1,2}-r_{AZ1,2})(r_{B,2}-r_{BZ2,2})w_{Z1}-m_{AZ1}m_{BA}m_{BZ2}r_{Z1,2}(r_{AB,2}-r_{B,2})(r_{A,2}-r_{AZ1,2})(r_{Z2,2}-r_{BZ2,2})w_{Z2})}$$
(S.5)

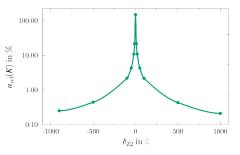
Mathematically, this approach would work but if uncertainties are also considered it becomes obvious that this method works only theoretically. In order to demonstrate this another simulation was performed. As example two-isotope system copper was chosen. The international reference material for copper is NIST 3114 [1], in this simulation it is material Z. The isotopic composition of material Z can assumed to be natural and was taken from de Laeter et al.<sup>[2]</sup> The isotopic composition of the second reference Z2 materiel, which is only hypothetical, was changed according to equation S.6, whereas  $x_{Z2} ({}^{65}Cu) = 1 - x_{Z2} ({}^{63}Cu)$ .  $\delta_{Z2}$  ranged from -900 % to 445 % (being the upper limit otherwise  $x_{Z2} ({}^{65}Cu)$  would be less than zero). The isotopic composition, the masses of the spike material A and B as well as the measured intensity ratios can be found in the EXCEL sheet accompanying this supplement. The K factor was estimated from an earlier measurement of the reference material NIST 885 [3] and assuming its isotopic composition to be natural. For each of the isotopic different materials Z2 the K-factor and is associated relative uncertainty  $u_{\rm rel}(K)$  was calculated as well as the relative deviation from the theoretical ("true") value, see equation S.7. The uncertainties were calculated via a Monte Carlo simulation following international recommendations [4] and using  $10^5$  trials. The results of this simulation are graphically shown in figure 1. Subfigure 1a shows the absolute value of  $\Delta_{\rm K}$  plotted against  $\delta_{\rm Z2}$ . The other subfigure shows  $u_{\rm rel}(K)$  also plotted against  $\delta_{\rm Z2}$ . Please mind the logarithmic y-scale used in both figures. From these two subfigures it becomes instantly clear, that the isotopic composition of Z2 must be significantly different from the composition of Z, otherwise the uncertainty associated with K becomes huge (in the worst case  $\approx 300 \%$  with  $\delta_{\rm Z2} = 0 \%$ ) and also a deviation from the true value can be witnessed. Only if  $|\delta_{Z2}|$  exceeds 400 \% both the relative uncertainty and the deviation from the true value get acceptable. A second reference material with a significantly

different isotopic composition is hardly the case for many elements and therefore using two reference materials is only a theoretical approach.

$$\delta_{\rm Z2} = \left(\frac{x_{\rm Z2} \,{\rm (}^{63}{\rm Cu}{\rm )}}{x_{\rm Z} \,{\rm (}^{63}{\rm Cu}{\rm )}} - 1\right) \cdot 1000 \,\%$$
(S.6)

$$\Delta_{K_2} = \left(\frac{K_{2,\text{calc}}}{K_{2,\text{true}}} - 1\right) \cdot 100\% \tag{S.7}$$





(a)  $|\Delta_{K_2}|$  as a function of  $\delta_{Z2}$ . Each point represents a Monte Carlo simulation with  $10^5$  trails.

(b)  $u_{\rm rel}(K_2)$  as a function of  $\delta_{\rm Z2}$ . Each point represents a Monte Carlo simulation with  $10^5$  trails.

Fig. 1: Results of investigation of the influence of the isotopic composition of the second reference material Z2 on the K itself and its associated uncertainty.

## 3 Step-by-Step Derivation of Equation 9

$$R_{\rm AB} = \frac{n_2}{n_1} = \frac{n_{\rm A} x_{\rm A,2} + n_{\rm B} x_{\rm B,2}}{n_{\rm A} x_{\rm A,1} + n_{\rm B} x_{\rm B,1}}$$
(S.8)

$$\beta_X = \frac{n_X}{m_X} \tag{S.9}$$

$$R_{\rm AB} = \frac{\beta_{\rm A} m_{\rm AB} x_{\rm A,2} + \beta_{\rm B} m_{\rm BA} x_{\rm B,2}}{\beta_{\rm A} m_{\rm AB} x_{\rm A,1} + \beta_{\rm B} m_{\rm BA} x_{\rm B,1}} \tag{S.10}$$

$$x_{X,2} = \frac{R_{X,2}}{R_{X,1} + R_{X,2}} = \frac{R_{X,2}}{1 + R_{X,2}}, X \in \{A, B, Z\}$$
(S.11)

$$R_{AB} = \frac{\beta_{A}m_{AB}\frac{R_{A,2}}{1+R_{A,2}} + \beta_{B}m_{BA}\frac{R_{B,2}}{1+R_{B,2}}}{\beta_{A}m_{AB}\frac{1}{1+R_{A,2}} + \beta_{B}m_{BA}\frac{1}{1+R_{B,2}}} = \frac{\beta_{A}m_{AB}\frac{R_{A,2}}{1+R_{A,2}} + \beta_{B}m_{BA}\frac{R_{B,2}}{1+R_{B,2}}}{\beta_{A}m_{AB}\frac{1}{1+R_{A,2}} + \beta_{B}m_{BA}\frac{1}{1+R_{B,2}}}$$
(S.12)

$$K_{2}r_{AB,2} = \frac{\beta_{A}m_{AB}\frac{K_{2}r_{A,2}}{1+K_{2}r_{A,2}} + \beta_{B}m_{BA}\frac{K_{2}r_{B,2}}{1+K_{2}r_{B,2}}}{\beta_{A}m_{AB}\frac{1}{1+K_{2}r_{A,2}} + \beta_{B}m_{BA}\frac{1}{1+K_{2}r_{B,2}}}$$
(S.13)

$$r_{AB,2} = \frac{\beta_A m_{AB} \frac{r_{A,2}}{1 + K_2 r_{A,2}} + \beta_B m_{BA} \frac{r_{B,2}}{1 + K_2 r_{B,2}}}{\beta_A m_{AB} \frac{1}{1 + K_2 r_{A,2}} + \beta_B m_{BA} \frac{1}{1 + K_2 r_{B,2}}}$$
(S.14)

$$r_{AB,2} \left( \beta_A m_{AB} \frac{1}{1 + K_2 r_{A,2}} + \beta_B m_{BA} \frac{1}{1 + K_2 r_{B,2}} \right) = \beta_A m_{AB} \frac{r_{A,2}}{1 + K_2 r_{A,2}} + \beta_B m_{BA} \frac{r_{B,2}}{1 + K_2 r_{B,2}}$$
(S.15)

$$\beta_{A}m_{AB}\frac{r_{AB,2}}{1+K_{2}r_{A,2}} + \beta_{B}m_{BA}\frac{r_{AB,2}}{1+K_{2}r_{B,2}} = \beta_{A}m_{AB}\frac{r_{A,2}}{1+K_{2}r_{A,2}} + \beta_{B}m_{BA}\frac{r_{B,2}}{1+K_{2}r_{B,2}}$$
(S.16)

$$(1 + K_2 r_{B,2}) r_{AB,2} \beta_A m_{AB} + (1 + K_2 r_{A,2}) r_{AB,2} \beta_B m_{BA} = (1 + K_2 r_{B,2}) r_{A,2} \beta_A m_{AB} + (1 + K_2 r_{A,2}) r_{B,2} \beta_B m_{BA}$$
(S.17)

 $r_{AB,2}\beta_{A}m_{AB} + K_{2}r_{B,2}r_{AB,2}\beta_{A}m_{AB} + r_{AB,2}\beta_{B}m_{BA} + K_{2}r_{A,2}r_{AB,2}\beta_{B}m_{BA} =$  $r_{A,2}\beta_{A}m_{AB} + K_{2}r_{B,2}r_{A,2}\beta_{A}m_{AB} + r_{B,2}\beta_{B}m_{BA} + K_{2}r_{A,2}r_{B,2}\beta_{B}m_{BA}$ (S.18)

$$\begin{split} K_2 r_{\mathrm{B},2} r_{\mathrm{AB},2} \beta_{\mathrm{A}} m_{\mathrm{AB}} + K_2 r_{\mathrm{A},2} r_{\mathrm{AB},2} \beta_{\mathrm{B}} m_{\mathrm{BA}} - K_2 r_{\mathrm{B},2} \beta_{\mathrm{A}} m_{\mathrm{AB}} - K_2 r_{\mathrm{A},2} r_{\mathrm{B},2} \beta_{\mathrm{B}} m_{\mathrm{BA}} = r_{\mathrm{A},2} \beta_{\mathrm{A}} m_{\mathrm{AB}} + r_{\mathrm{B},2} \beta_{\mathrm{B}} m_{\mathrm{BA}} - r_{\mathrm{AB},2} \beta_{\mathrm{A}} m_{\mathrm{AB}} - r_{\mathrm{AB},2} \beta_{\mathrm{B}} m_{\mathrm{BA}} = r_{\mathrm{AB},2} \beta_{\mathrm{B}} m_{\mathrm{BA}} - r_{\mathrm{AB},2} \beta_{\mathrm{B}} m_{\mathrm{AB},2} \beta_{\mathrm{B},2} \beta_{\mathrm{A},2} \beta_{\mathrm{B},2} \beta_{\mathrm{B$$

$$K_{2} \left(\beta_{A} m_{AB} \left(r_{B,2} r_{AB,2} - r_{B,2} r_{A,2}\right) + \beta_{B} m_{BA} \left(r_{A,2} r_{AB,2} - r_{A,2} r_{B,2}\right)\right) = \beta_{A} m_{AB} \left(r_{A,2} - r_{AB,2}\right) + \beta_{B} m_{BA} \left(r_{B,2} - r_{AB,2}\right)$$
(S.20)

$$K_{2} = \frac{\beta_{\rm A} m_{\rm AB} \left( r_{\rm A,2} - r_{\rm AB,2} \right) + \beta_{\rm B} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} \right)}{\beta_{\rm A} m_{\rm AB} \left( r_{\rm B,2} - r_{\rm B,2} - r_{\rm B,2} r_{\rm A,2} \right) + \beta_{\rm B} m_{\rm BA} \left( r_{\rm A,2} r_{\rm AB,2} - r_{\rm A,2} r_{\rm B,2} \right)}$$
(9)

# 4 Step-by-Step Derivation of Equations 19 and 20

$$\beta_{\rm Z} \equiv \frac{n_{\rm Z}}{m_{\rm Z}} \tag{S.21}$$

$$\beta_{\rm Z} = \frac{w_{\rm Z}}{M_{\rm Z}} \tag{S.22}$$

$$M_{\rm Z} = x_{\rm Z,1} M_1 + x_{\rm Z,2} M_2 \tag{S.23}$$

$$\beta_{\rm Z} = \frac{w_{\rm Z}}{\frac{1}{1+R_{\rm Z,2}}M_1 + \frac{R_{\rm Z,2}}{1+R_{\rm Z,2}}M_2} = \frac{w_{\rm Z}}{\frac{1}{1+R_{\rm Z,2}}(M_1 + R_{\rm Z,2}M_2)} = \frac{w_{\rm Z}(1+R_{\rm Z,2})}{M_1 + R_{\rm Z,2}M_2} = \frac{w_{\rm Z}(1+R_{\rm Z,2})}{w_{\rm Z}(1+R_{\rm Z,2}M_2)}$$
(S.24)

$$\frac{w_{\rm Z} \left(1 + M_2 r_{\rm Z,2}\right)}{M_1 + K_2 r_{\rm Z,2} M_2}$$

$$A_{\rm Z} = k_{\rm Z} \beta_{\rm Z} \frac{m_{\rm ZY}}{m_{\rm sln,Z}} \tag{S.25}$$

$$A_{\rm YZ} = k_{\rm YZ} \beta_{\rm Y} \frac{m_{\rm YZ}}{m_{\rm sln,Z}} \tag{S.26}$$

$$A_X = k_X \beta_X \frac{m_{\rm XY}}{m_{\rm sln,X}} \tag{S.27}$$

$$A_{\rm YX} = k_{\rm YX} \beta_{\rm Y} \frac{m_{\rm YX}}{m_{{\rm sln},X}} \tag{S.28}$$

$$f_{\rm Z} = \frac{A_{\rm Z}}{A_{\rm YZ}} = \frac{k_{\rm Z}}{k_{\rm YZ}} \frac{\beta_{\rm Z}}{\beta_{\rm Y}} \frac{m_{\rm ZY}}{m_{\rm YZ}} \tag{S.29}$$

$$f_X = \frac{A_X}{A_{\rm YX}} = \frac{k_X}{k_{\rm YX}} \frac{\beta_X}{\beta_{\rm Y}} \frac{m_{\rm XY}}{m_{\rm YX}}$$
(S.30)

$$\beta_X = \frac{k_{\rm YX}}{k_X} f_X \beta_{\rm Y} \frac{m_{\rm YX}}{m_{\rm XY}} \tag{S.31}$$

 $\mathbf{5}$ 

$$\frac{k_{\rm YX}}{k_X} = \frac{k_{\rm YZ}}{k_Z} = \frac{1}{f_Z} \frac{\beta_Z}{\beta_Y} \frac{m_{\rm ZY}}{m_{\rm YZ}}$$
(S.32)

$$\beta_X = \frac{1}{f_Z} \frac{\beta_Z}{\beta_Y} \frac{m_{ZY}}{m_{YZ}} f_X \beta_Y \frac{m_{YX}}{m_{XY}}$$
(S.33)

$$\beta_X = \beta_Z \frac{m_{ZY}}{m_{YZ}} \frac{m_{YX}}{m_{XY}} \frac{f_X}{f_Z}, \text{ with } X \in \{A, B\},$$
(S.34)

Inserting S.24.

$$\beta_X = w_Z \frac{1 + K_2 r_{Z,2}}{M_1 + K_2 r_{Z,2} M_2} \frac{m_{ZY}}{m_{YZ}} \frac{m_{YX}}{m_{XY}} \frac{f_X}{f_Z}, \text{ with } X \in \{A, B\}$$
(19 & 20)

## 5 Step-by-Step Derivation of Equation 21

Starting from equation S.7, which can be rearranged to:

$$\beta_{\rm A}m_{\rm AB} \left( r_{\rm AB,2} - r_{\rm A,2} + K_2 \left( r_{\rm B,2}r_{\rm AB,2} - r_{\rm B,2}r_{\rm A,2} \right) \right) = \beta_{\rm B}m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} + K_2 \left( r_{\rm A,2}r_{\rm B,2} - r_{\rm A,2}r_{\rm AB,2} \right) \right)$$
(S.35)

Now  $\beta_{\rm A}$  and  $\beta_{\rm B}$  an be replaced with equations 19 and 20, respectively.

$$w_{\rm Z} \frac{1 + K_2 r_{\rm Z,2}}{M_1 + K_2 r_{\rm Z,2} M_2} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{m_{\rm YA}}{m_{\rm YZ}} \frac{f_{\rm A}}{f_{\rm Z}} m_{\rm AB} \left( r_{\rm AB,2} - r_{\rm A,2} + K_2 \left( r_{\rm B,2} r_{\rm AB,2} - r_{\rm B,2} r_{\rm A,2} \right) \right) = w_{\rm Z} \frac{1 + K_2 r_{\rm Z,2}}{M_1 + K_2 r_{\rm Z,2} M_2} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} + K_2 \left( r_{\rm A,2} r_{\rm B,2} - r_{\rm A,2} r_{\rm A,2} r_{\rm B,2} \right) \right) = K_2 \frac{1 + K_2 r_{\rm Z,2}}{M_1 + K_2 r_{\rm Z,2} M_2} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} + K_2 \left( r_{\rm A,2} r_{\rm B,2} - r_{\rm A,2} r_{\rm A,2} r_{\rm A,2} \right) \right) = K_2 \frac{1 + K_2 r_{\rm Z,2}}{M_1 + K_2 r_{\rm Z,2} M_2} \frac{m_{\rm YZ}}{m_{\rm YZ}} \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} + K_2 \left( r_{\rm A,2} r_{\rm B,2} - r_{\rm A,2} r_{\rm A,2} r_{\rm A,2} \right) \right)$$

This expression can then be solved for  $K_2$ .

$$\frac{m_{\rm YA}}{m_{\rm AY}} \frac{f_{\rm A}}{f_{\rm Z}} m_{\rm AB} \left( r_{\rm AB,2} - r_{\rm A,2} + K_2 \left( r_{\rm B,2} r_{\rm AB,2} - r_{\rm B,2} r_{\rm A,2} \right) \right) = \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} + K_2 \left( r_{\rm A,2} r_{\rm B,2} - r_{\rm A,2} r_{\rm AB,2} \right) \right) \tag{S.37}$$

$$\frac{m_{\rm YA}}{m_{\rm AY}} \frac{f_{\rm A}}{f_{\rm Z}} m_{\rm AB} \left( r_{\rm AB,2} - r_{\rm A,2} \right) + K_2 \left( r_{\rm B,2} r_{\rm AB,2} - r_{\rm B,2} r_{\rm A,2} \right) \frac{m_{\rm YA}}{m_{\rm AY}} \frac{f_{\rm A}}{f_{\rm Z}} m_{\rm AB} = \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} \right) + K_2 \left( r_{\rm A,2} r_{\rm B,2} - r_{\rm A,2} r_{\rm AB,2} \right) \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}} m_{\rm BA}$$
(S.38)

$$K_{2}\left(\frac{m_{\rm YA}}{m_{\rm AY}}\frac{f_{\rm A}}{f_{\rm Z}}m_{\rm AB}\left(r_{\rm B,2}r_{\rm AB,2} - r_{\rm B,2}r_{\rm A,2}\right) + \frac{m_{\rm YB}}{m_{\rm BY}}\frac{f_{\rm B}}{f_{\rm Z}}m_{\rm BA}\left(r_{\rm A,2}r_{\rm AB,2} - r_{\rm A,2}r_{\rm B,2}\right)\right) = \frac{m_{\rm YA}}{m_{\rm AY}}\frac{f_{\rm A}}{f_{\rm Z}}m_{\rm AB}\left(r_{\rm A,2} - r_{\rm AB,2}\right) + \frac{m_{\rm YB}}{m_{\rm BY}}\frac{f_{\rm B}}{f_{\rm Z}}m_{\rm BA}\left(r_{\rm B,2} - r_{\rm A}\frac{g_{\rm B}}{g_{\rm B}}\right)$$

$$K_{2} = \frac{\frac{m_{\rm YA}}{m_{\rm AY}} \frac{f_{\rm A}}{f_{\rm Z}} m_{\rm AB} \left(r_{\rm A,2} - r_{\rm AB,2}\right) + \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}} m_{\rm BA} \left(r_{\rm B,2} - r_{\rm AB,2}\right)}{\frac{m_{\rm YA}}{m_{\rm AY}} \frac{f_{\rm A}}{f_{\rm Z}} m_{\rm AB} \left(r_{\rm B,2} r_{\rm AB,2} - r_{\rm B,2} r_{\rm A,2}\right) + \frac{m_{\rm YB}}{m_{\rm BY}} \frac{f_{\rm B}}{f_{\rm Z}} m_{\rm BA} \left(r_{\rm A,2} r_{\rm AB,2} - r_{\rm A,2} r_{\rm B,2}\right)}$$
(S.40)

$$K_{2} = \frac{\frac{m_{\rm YA}}{m_{\rm AY}} f_{\rm A} m_{\rm AB} \left( r_{\rm A,2} - r_{\rm AB,2} \right) + \frac{m_{\rm YB}}{m_{\rm BY}} f_{\rm B} m_{\rm BA} \left( r_{\rm B,2} - r_{\rm AB,2} \right)}{\frac{m_{\rm YA}}{m_{\rm AY}} f_{\rm A} m_{\rm AB} \left( r_{\rm B,2} r_{\rm AB,2} - r_{\rm B,2} r_{\rm A,2} \right) + \frac{m_{\rm YB}}{m_{\rm BY}} f_{\rm B} m_{\rm BA} \left( r_{\rm A,2} r_{\rm AB,2} - r_{\rm A,2} r_{\rm B,2} \right)}$$
(21)

## 6 Explicit Solutions of $w_{\rm A}$ and $w_{\rm B}$

Now we show how equation 22 can be obtained, equation 23 is derived analogously. We recall the following equations from the main manuscript:

$$\beta_{\rm A} = w_{\rm Z} \frac{1 + K_2 r_{\rm Z,2}}{M_1 + K_2 r_{\rm Z,2} M_2} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{m_{\rm YA}}{m_{\rm AY}} \frac{f_{\rm A}}{f_{\rm Z}}$$
(19)

as well as:

$$M_{\rm A} = \frac{M_1 + K \times r_{\rm A,2} M_2}{1 + K \times r_{\rm A,2}} \tag{S.41}$$

and

$$w_{\rm A} = \beta_{\rm A} M_{\rm A} \tag{S.42}$$

Inserting equations 19 and S.41 into equation S.42 leads to equation 22. By inserting equation 21 in equations 22 and 23 (main manuscript) the following expressions can be obtained.

$$w_{A} = w_{Z} \frac{m_{ZY}}{m_{YZ}} \frac{f_{A}m_{AB}m_{BY}m_{YA} (r_{A,2} - r_{AB,2}) (r_{A,2}M_{2} - r_{B,2}M_{1}) + f_{B}m_{BA}m_{AY}m_{YB} (r_{A,B,2} - r_{B,2}) (r_{A,2}M_{1} - r_{A,2}M_{2})}{f_{Z}m_{AB}m_{AY}m_{BY} (r_{A,2} - r_{AB,2}) (r_{A,2} - r_{B,2}) (r_{A,2} - r_{B,2})} + \frac{f_{A}m_{AB}m_{BY}m_{YA} (r_{A,2} - r_{AB,2}) (r_{B,2} - r_{Z,2}) - f_{B}m_{BA}m_{AY}m_{YB} (r_{A,B,2} - r_{B,2}) (r_{A,2} - r_{Z,2})}{f_{A}m_{AB}m_{BY}m_{YA} (r_{A,2} - r_{AB,2}) (r_{B,2}M_{1} - r_{Z,2}M_{2}) - f_{B}m_{BA}m_{AY}m_{YB} (r_{AB,2} - r_{B,2}) (r_{A,2} - r_{Z,2})}$$

$$(S.43)$$

$$w_{\rm B} = w_{\rm Z} \frac{m_{\rm ZY}}{m_{\rm YZ}} \frac{f_{\rm B} m_{\rm BA} m_{\rm AY} m_{\rm YB} \left(r_{\rm B,2} - r_{\rm AB,2}\right) \left(r_{\rm B,2} M_2 - r_{\rm A,2} M_1\right) + f_{\rm A} m_{\rm AB} m_{\rm BY} m_{\rm YA} \left(r_{\rm AB,2} - r_{\rm A,2}\right) \left(r_{\rm B,2} M_1 - r_{\rm B,2} M_2\right)}{f_{\rm Z} m_{\rm BA} m_{\rm BY} m_{\rm AY} \left(r_{\rm B,2} - r_{\rm A,2}\right) \left(r_{\rm B,2} - r_{\rm A,2}\right)} \frac{r_{\rm B,2} m_{\rm BA} m_{\rm BY} m_{\rm AY} \left(r_{\rm B,2} - r_{\rm A,2}\right)}{f_{\rm B} m_{\rm BA} m_{\rm AY} m_{\rm YB} \left(r_{\rm B,2} - r_{\rm AB,2}\right) \left(r_{\rm A,2} - r_{\rm Z,2}\right) - f_{\rm A} m_{\rm BB} m_{\rm BY} m_{\rm YA} \left(r_{\rm AB,2} - r_{\rm A,2}\right) \left(r_{\rm B,2} - r_{\rm Z,2}\right)} \right)} \left( S.44 \right)$$

## 7 Generalization

In this section it is shown how the generalized formulas in the main manuscript (equations 25 and 27) were derived. In order to do so a three-isotope system is considered. According to equation 8 the measured ratios of the two necessary blends (AB and AC) can be expressed as:

$$r_{AB,2} = \frac{f_A m_{AB} m_{BY} m_{YA} r_{A,2} (K_2 r_{B,2} + K_3 r_{B,3} + 1) +}{f_B m_{AY} m_{BA} m_{YB} r_{B,2} (K_2 r_{A,2} + K_3 r_{A,3} + 1)} \\ f_A m_{AB} m_{BY} m_{YA} (K_2 r_{B,2} + K_3 r_{B,3} + 1) +} \\ f_B m_{AY} m_{BA} m_{YB} (K_2 r_{A,2} + K_3 r_{A,3} + 1)$$
(S.45)

and

$$r_{\rm AC,2} = \frac{f_{\rm A}m_{\rm AC}m_{\rm CY}m_{\rm YA}r_{\rm A,2}(K_2r_{\rm C,2} + K_3r_{\rm C,3} + 1) + f_{\rm C}m_{\rm AY}m_{\rm CA}m_{\rm YC}r_{\rm C,2}(K_2r_{\rm A,2} + K_3r_{\rm A,3} + 1)}{f_{\rm A}m_{\rm AC}m_{\rm CY}m_{\rm YA}(K_2r_{\rm C,2} + K_3r_{\rm C,3} + 1) + f_{\rm C}m_{\rm AY}m_{\rm CA}m_{\rm YC}(K_2r_{\rm A,2} + K_3r_{\rm A,3} + 1)}$$
(S.46)

The last two equations can be rearranged, leading to:

$$r_{AB,2}(f_A m_{AB} m_{BY} m_{YA} (K_2 r_{B,2} + K_3 r_{B,3} + 1) + f_B m_{AY} m_{BA} m_{YB} (K_2 r_{A,2} + K_3 r_{A,3} + 1)) = f_A m_{AB} m_{BY} m_{YA} r_{A,2} (K_2 r_{B,2} + K_3 r_{B,3} + 1) + f_B m_{AY} m_{BA} m_{YB} r_{B,2} (K_2 r_{A,2} + K_3 r_{A,3} + 1))$$
(S.47)

and

$$r_{AC,2}(f_A m_{AC} m_{CY} m_{YA} (K_2 r_{C,2} + K_3 r_{C,3} + 1) + f_C m_{AY} m_{CA} m_{YC} (K_2 r_{A,2} + K_3 r_{A,3} + 1)) = f_A m_{AC} m_{CY} m_{YA} r_{A,2} (K_2 r_{C,2} + K_3 r_{C,3} + 1) + f_C m_{AY} m_{CA} m_{YC} r_{C,2} (K_2 r_{A,2} + K_3 r_{A,3} + 1))$$
(S.48)

In the next step some quantities  $(K_2, K_3, f_A, f_B, C, m_{AB}, m_{AC}, m_{AD}, m_{BA}, m_{CA}, m_{YA}, m_{AY}, m_{BY}, m_{YB}, m_{YC}, m_{CY})$  in both expressions can be collected. This leads to:

 $f_{A}m_{AB}m_{BY}m_{YA}r_{AB,2} + f_{B}m_{AY}m_{BA}m_{YB}r_{AB,2}$   $+K_{2}(f_{B}m_{AY}m_{BA}m_{YB}r_{A,2}r_{AB,2} + f_{A}m_{AB}m_{BY}m_{YA}r_{AB,2}r_{B,2})$   $+K_{3}(f_{B}m_{AY}m_{BA}m_{YB}r_{A,3}r_{AB,2} + f_{A}m_{AB}m_{BY}m_{YA}r_{AB,2}r_{B,3}) =$   $f_{A}m_{AB}m_{BY}m_{YA}r_{A,2} + f_{B}m_{AY}m_{BA}m_{YB}r_{B,2}$   $+K_{2}(f_{A}m_{AB}m_{BY}m_{YA}r_{A,2}r_{B,2} + f_{B}m_{AY}m_{BA}m_{YB}r_{A,2}r_{B,2}) \quad (S.49)$   $+K_{3}(f_{B}m_{AY}m_{BA}m_{YB}r_{A,3}r_{B,2} + f_{A}m_{AB}m_{BY}m_{YA}r_{A,2}r_{B,3})$ 

and

$$f_{A}m_{AC}m_{CY}m_{YA}r_{AC,2} + f_{C}m_{AY}m_{CA}m_{YC}r_{AC,2}$$
$$+K_{2}(f_{C}m_{AY}m_{CA}m_{YC}r_{A,2}r_{AC,2} + f_{A}m_{AC}m_{CY}m_{YA}r_{AC,2}r_{C,2})$$
$$+K_{3}(f_{C}m_{AY}m_{CA}m_{YC}r_{A,3}r_{AC,2} + f_{A}m_{AC}m_{CY}m_{YA}r_{AC,2}r_{C,3}) =$$

 $f_{A}m_{AC}m_{CY}m_{YA}r_{A,2} + f_{C}m_{AY}m_{CA}m_{YC}r_{C,2}$  $+ K_2(f_{A}m_{AC}m_{CY}m_{YA}r_{A,2}r_{C,2} + f_{C}m_{AY}m_{CA}m_{YC}r_{A,2}r_{C,2})$ (S.50) +  $K_3(f_{C}m_{AY}m_{CA}m_{YC}r_{A,3}r_{C,2} + f_{A}m_{AC}m_{CY}m_{YA}r_{A,2}r_{C,3})$ 

Now all terms containing one of the two K-factors are collected on one side and the others on the other side, this leads to:

$$K_{2}(f_{B}(m_{AY}m_{BA}m_{YB}r_{A,2}r_{AB,2} - m_{AY}m_{BA}m_{YB}r_{A,2}r_{B,2}) + f_{A}(m_{AB}m_{BY}m_{YA}r_{AB,2}r_{B,2} - m_{AB}m_{BY}m_{YA}r_{A,2}r_{B,2})) + K_{3}(f_{B}(m_{AY}m_{BA}m_{YB}r_{A,3}r_{AB,2} - m_{AY}m_{BA}m_{YB}r_{A,3}r_{B,2}) + f_{A}(m_{AB}m_{BY}m_{YA}r_{AB,2}r_{B,3} - m_{AB}m_{BY}m_{YA}r_{A,2}r_{B,3})) = f_{A}(m_{AB}m_{BY}m_{YA}r_{A,2} - m_{AB}m_{BY}m_{YA}r_{AB,2}) + f_{B}(m_{AY}m_{BA}m_{YB}r_{B,2} - m_{AY}m_{BA}m_{YB}r_{AB,2}) + f_{B}(m_{AY}m_{BA}m_{YB}r_{B,2} - m_{AY}m_{BA}m_{YB}r_{AB,2}) K_{2}(f_{C}(m_{AY}m_{CA}m_{YC}r_{A,2}r_{C,2} - m_{AY}m_{CA}m_{YC}r_{A,2}r_{C,2})) + K_{3}(f_{C}(m_{AY}m_{CA}m_{YC}r_{A,3}r_{AC,2} - m_{AY}m_{CA}m_{YC}r_{A,3}r_{C,2}) + f_{A}(m_{AC}m_{CY}m_{YA}r_{AC,2}r_{C,3} - m_{AC}m_{CY}m_{YA}r_{A,2}r_{C,3}))$$
(S.51)

 $= f_{\rm A}(m_{\rm AC}m_{\rm CY}m_{\rm YA}r_{\rm A,2} - m_{\rm AC}m_{\rm CY}m_{\rm YA}r_{\rm AC,2}) + f_{\rm C}(m_{\rm AY}m_{\rm CA}m_{\rm YC}r_{\rm C,2} - m_{\rm AY}m_{\rm CA}m_{\rm YC}r_{\rm AC,2})$ 

The last two equations allow to determine the generic formulas given in the main manuscript.

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