
Electromagnetic Modelling of Time-Variant Propagation Effects due to Rotating Wind Turbines

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Overview

- Background: Influence of Wind Turbines on Operation of Air Surveillance Radar Systems
- Introduction: Measurement Campaigns
 - Ground Measurements
 - Commercial Hexacopter
- Electromagnetic Simulations of Wind Farm Scenarios
 - Ray Tracing Approach
 - Setup of Scenarios
 - Typical Results (Frequency Domain)
- Evaluation of Simulation Data in Time Domain
- Summary and Conclusions

Measurement Equipment



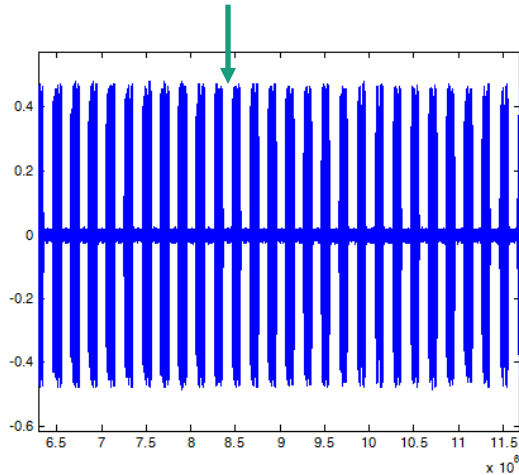
Ground measurements

FHR experimental airplane „Delphin“



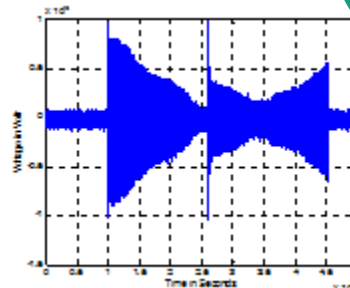
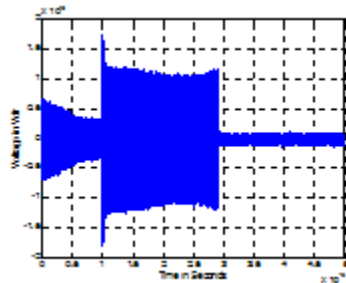
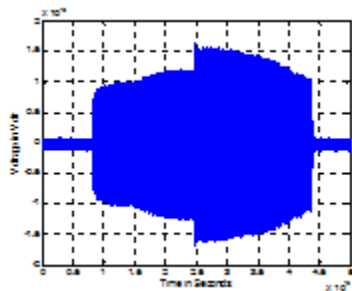
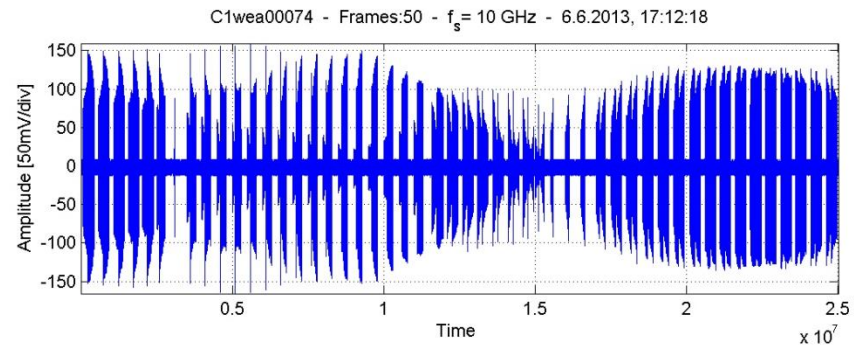
Typical Measurement Results

Without WEA in propagation path:
- Typical pulse series obtained



Typical Observations behind WEAs:

- Fluctuations of pulse power over time
- Change of pulse modulation caused by WEA
- Effects observed in different measurements



With WEA in propagation path:

- Typical pulse series
- Typical pulse modulations

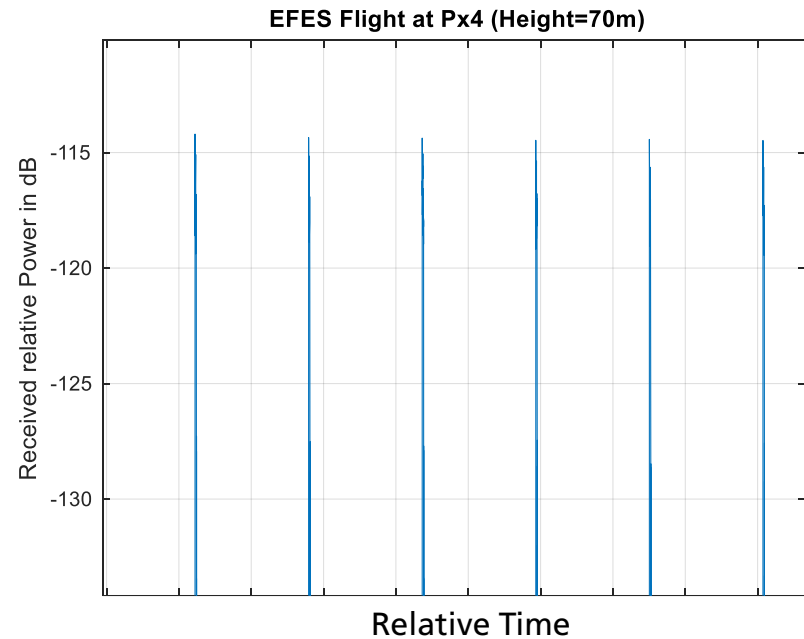
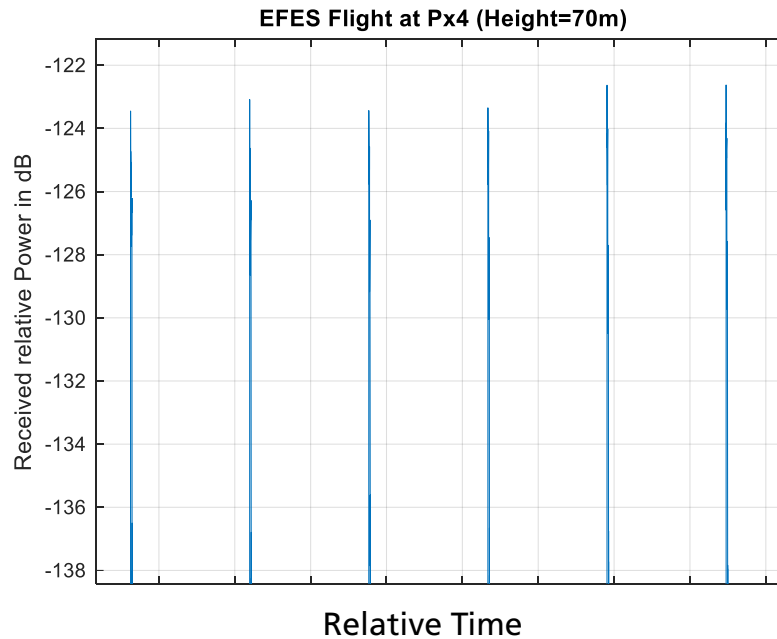
Measurements Using a Hexacopter

Measurement Platform:

- Commercially available hexacopter
- Control unit and receiver system designed for the measurements
- Field strengths at several locations have been recorded at different heights (max. 100 m)
- Antenna turned towards the air surveillance radar automatically
- Constant position during recording of field strength data
- Each data set covers a time frame including several pulses transmitted by the radar (corresponding to a very short cut through the simulated data)



Measurement Results (1)



Results at 70m height:

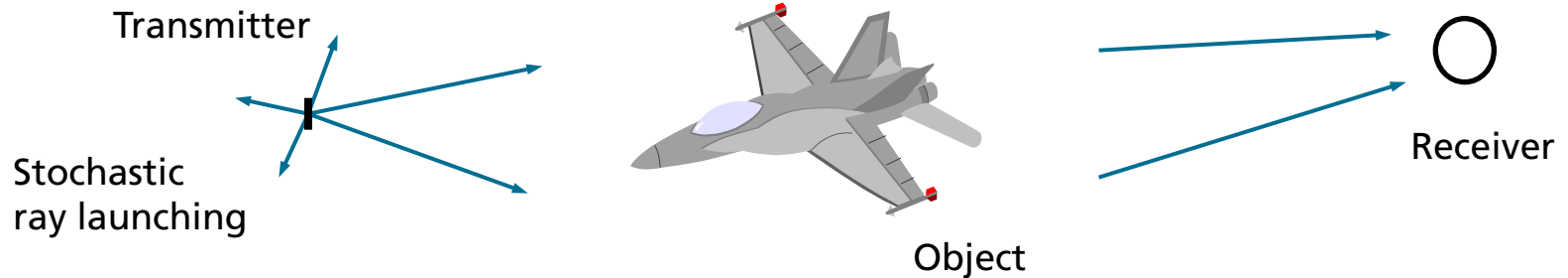
- Same height but during two different measurement sequences (corresponding to different rotation angles)
- Relative difference of 8 dB
- Good agreement of field strength variation with simulated data

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Simulation Approach

EM Fields Calculation with SBR Ray Tracing



Ray Tracing Method:

(Geometrical Calculation of Propagation Paths)

Shooting-and-Bouncing Rays (SBR), number of reflections practically unlimited

Discrete rays as representatives of ray tubes

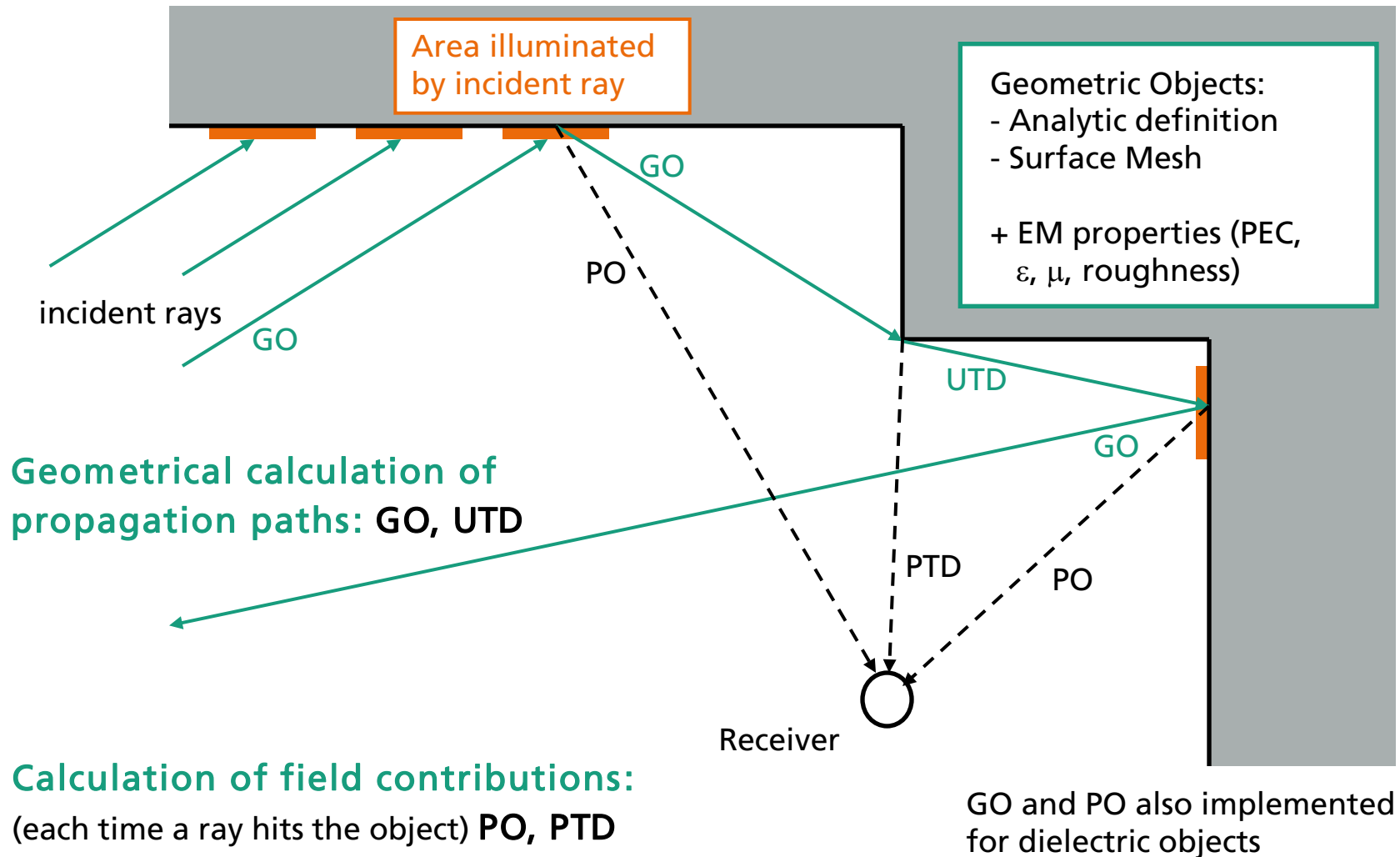
Ray-Density Normalisation (RDN) states the “distance” between rays

Calculation of Field Strength Contributions to Receiver:

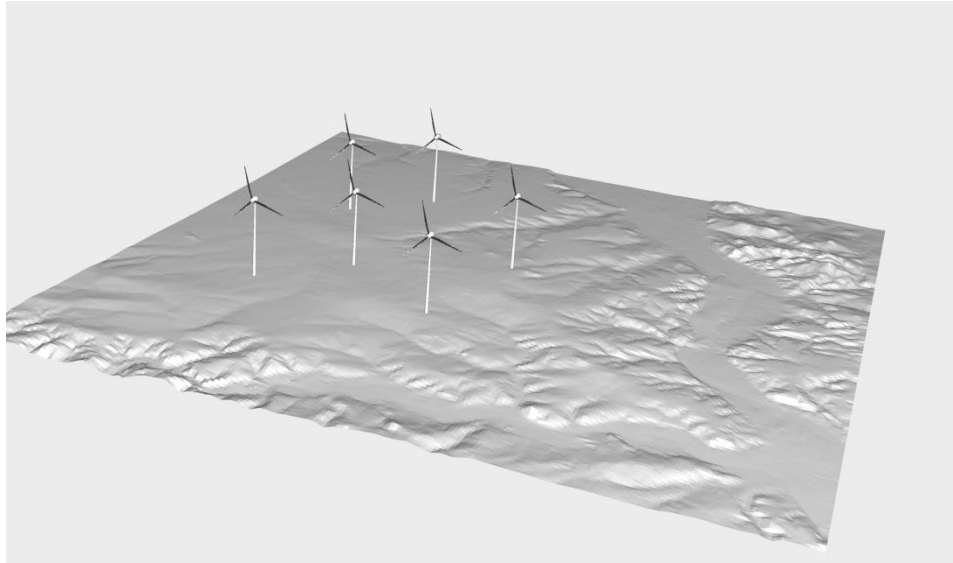
(each time a ray hits the object)

Physical Optics (PO) + Physical Theory of Diffraction (PTD)

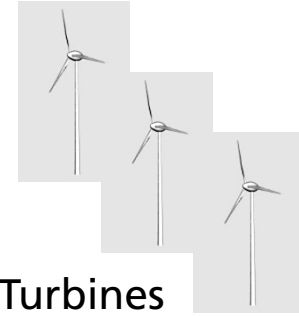
Ray Tracing: Combination of GO/UTD-PO/PTD



Schematic Setup of Simulations



Terrain (CAD-Model in NASTRAN format)



Wind Turbines
(CAD-Model in NASTRAN format)

Transmitter Specification
(Location, main lobe direction)

Receiver Specification
(Single point, 1D, 2D arrays,...)

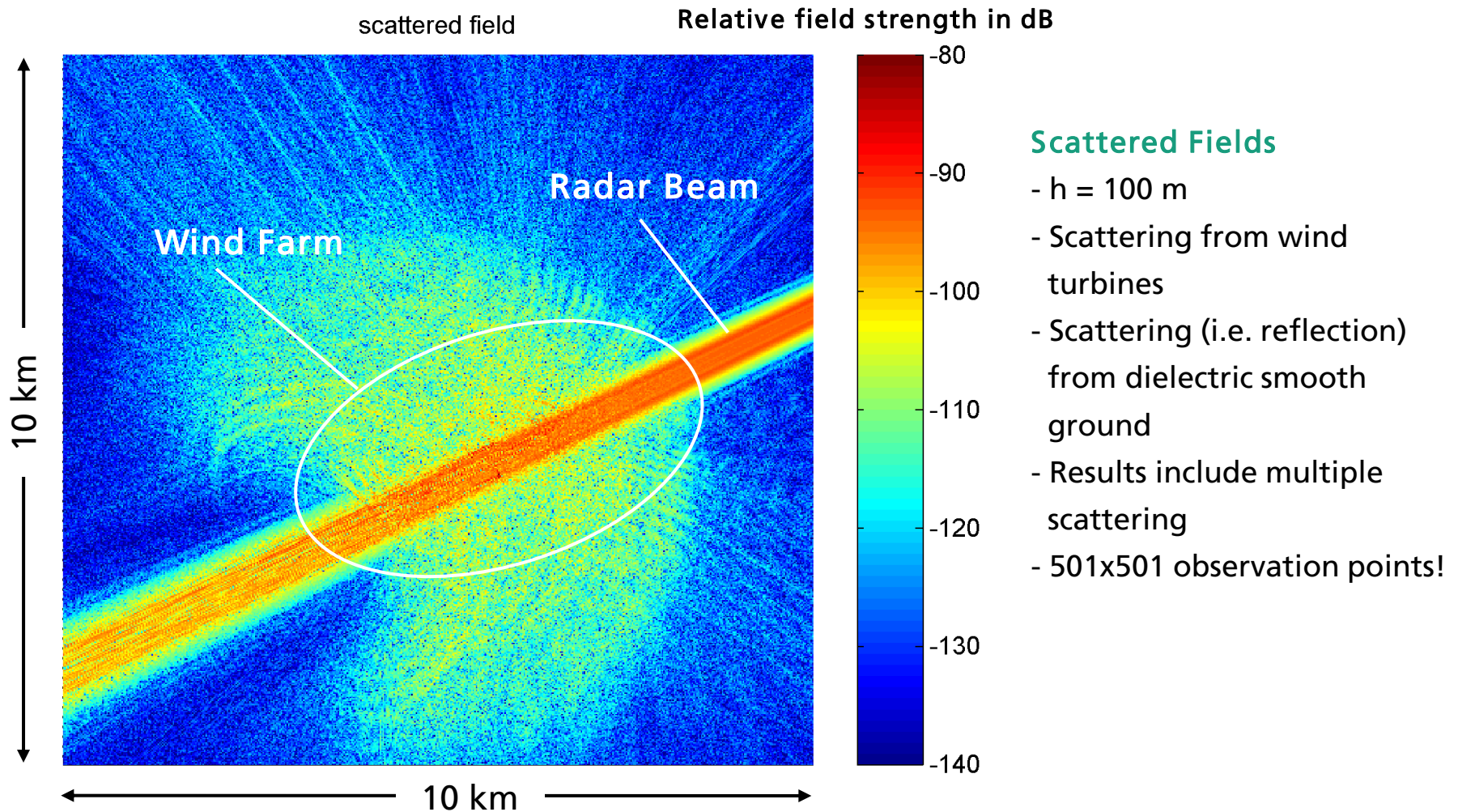


Ray Tracing Simulation

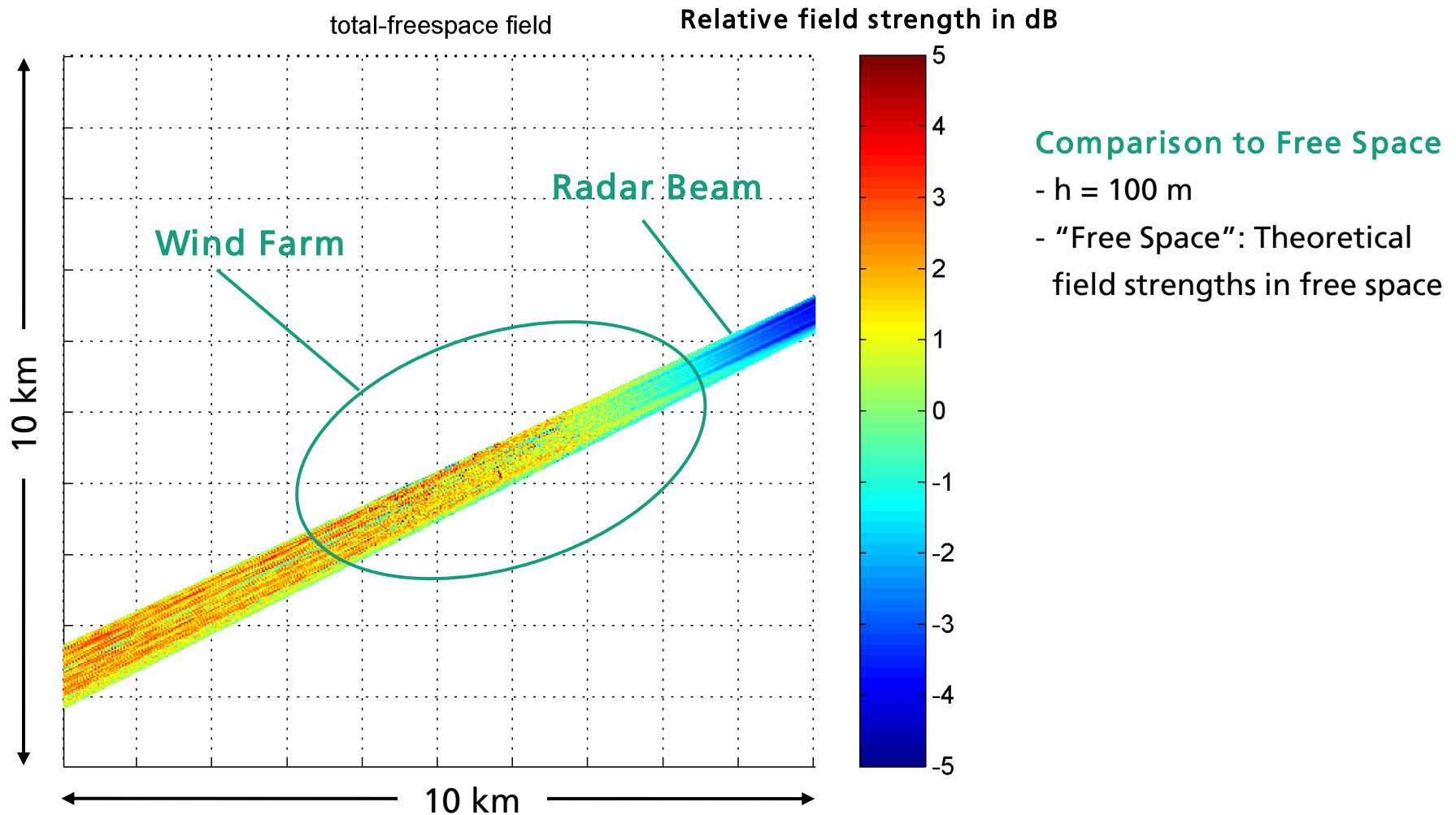


Output / Postprocessing:
Field Strengths
(Single point, 1D, 2D arrays,...)

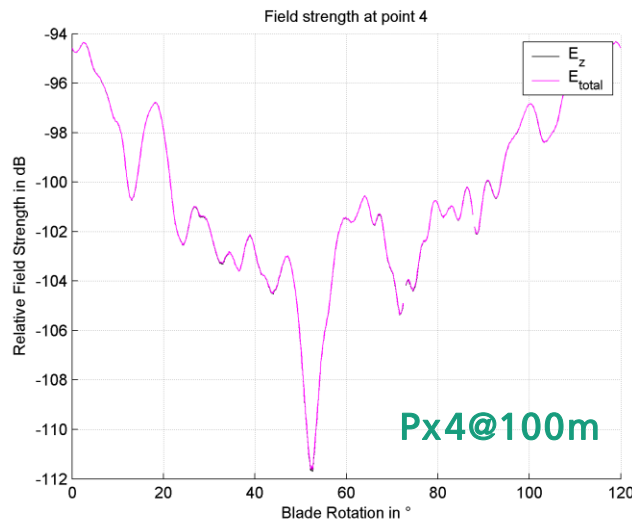
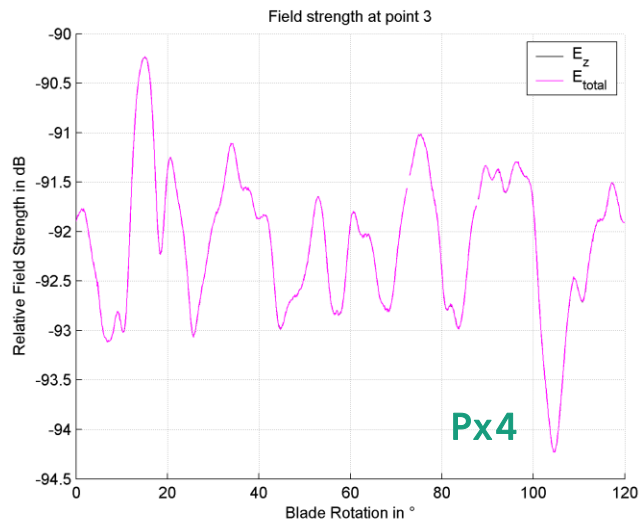
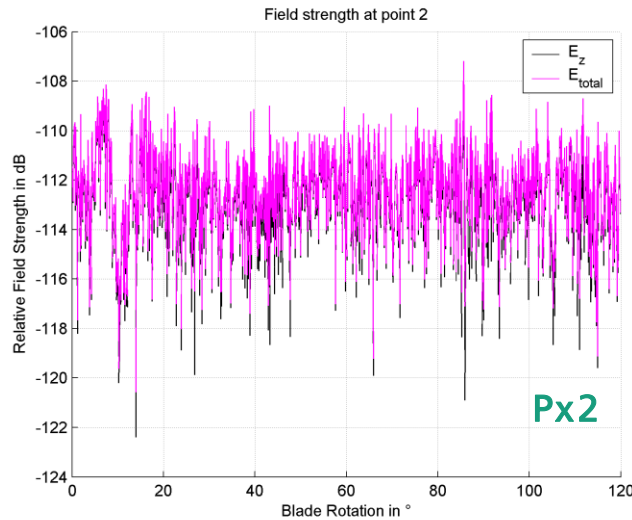
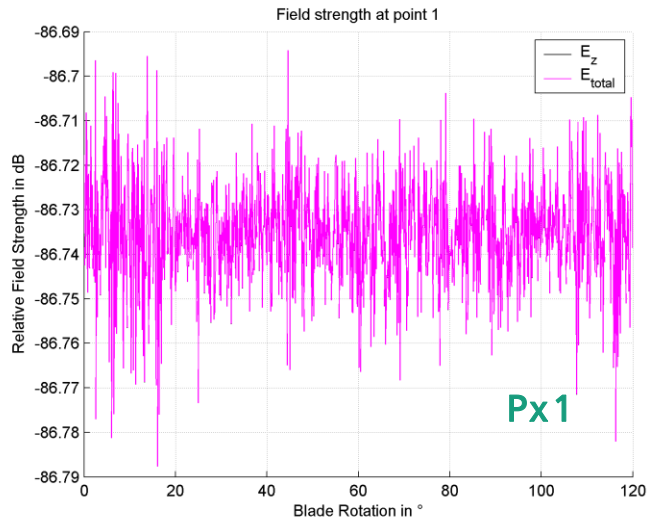
Wind Farm, Static Scenario (2D Field Distribution)



Simulation Results for Wind Farm (2D Field Distribution)



Wind Farm, Rotating Blades



Simulation Setup:

- Fixed observation points; sequence of quasi-static scenarios

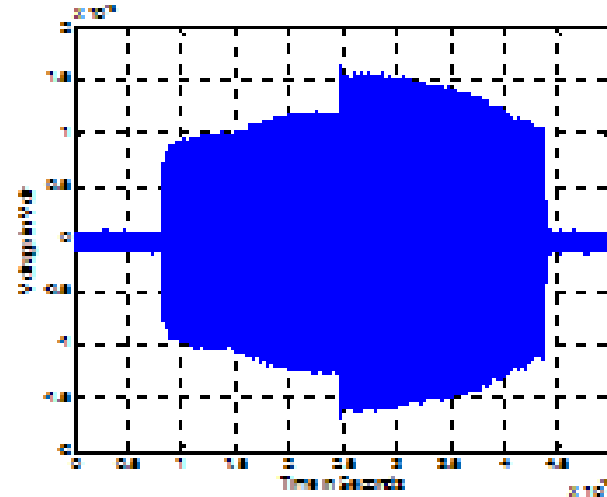
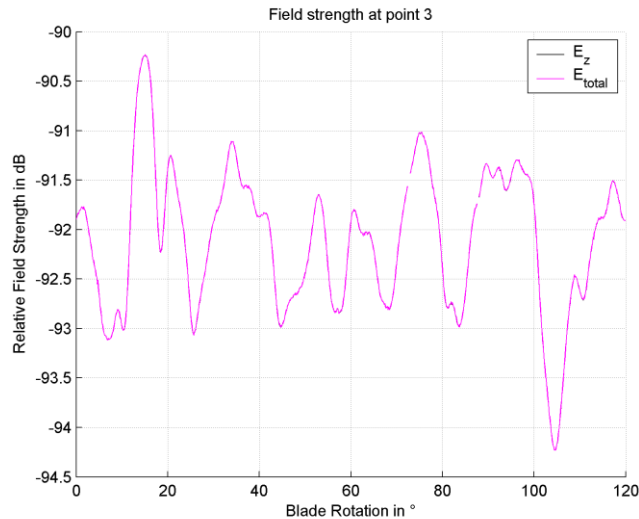
Observation:

- Simulation data show variation of field strengths, similar behavior as in measurements
- Variation of field strength also for distant (50km, 100km) observation points

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How to Compare Simulated and Measured Data



Simulated Data:

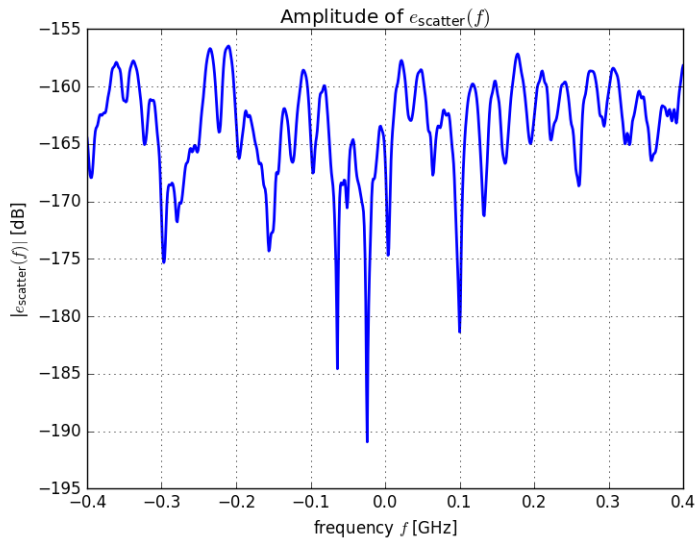
- Approach 1: Sequence of data in frequency domain

Measured Data:

- Pulse modulation in time domain

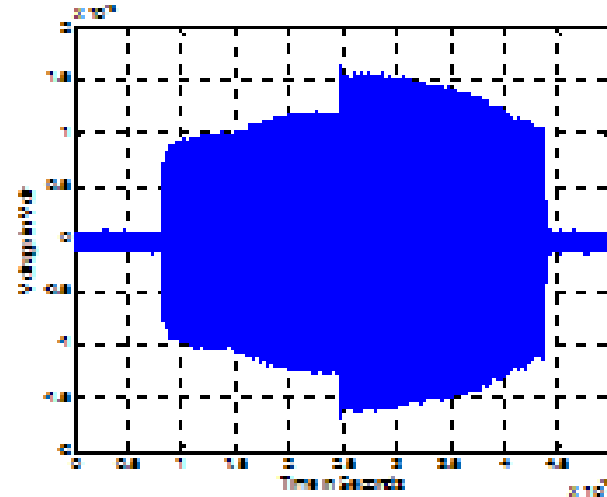
Results not exactly comparable

How to Compare Simulated and Measured Data



Simulated Data:

- Approach 2: N frequency data points
- Bandwidth: $(N-1) \Delta f$
- covered time window: $T = (N-1) \Delta t$, should be large enough to contain the scattered pulse, which leads to a minimum number of frequency data points



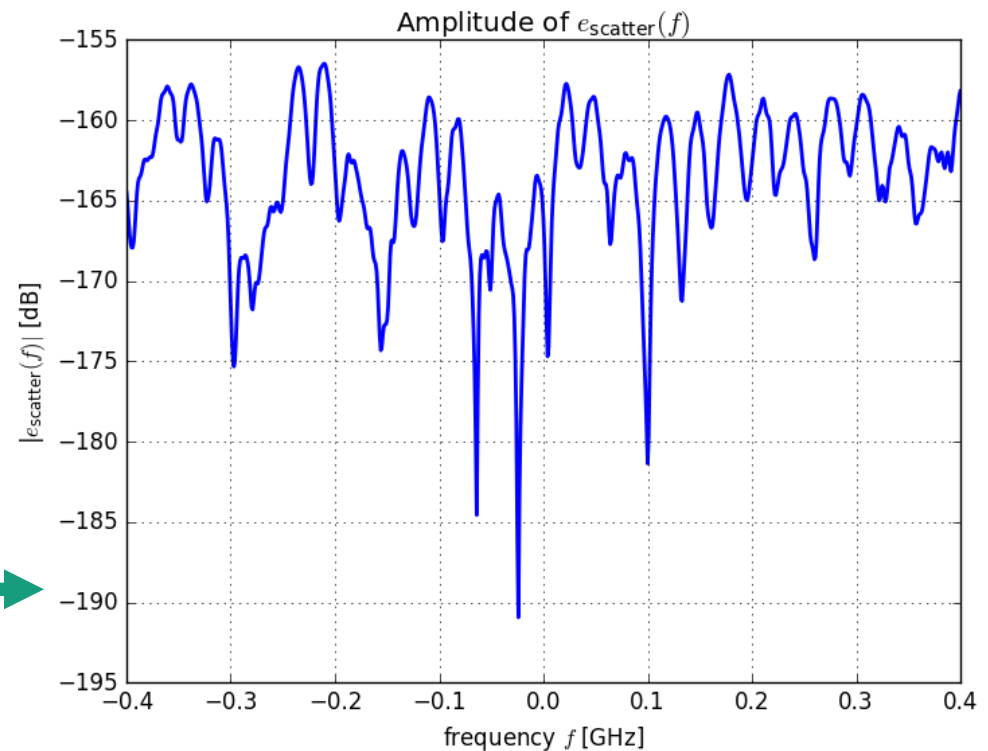
Measured Data:

- Pulse modulation in **time domain**

Simulation of Scattered Fields in Frequency Domain



Ray Tracing Simulation



Simulation Data:

- Frequency Domain Method (GO+PO)
- Can be provided for a given bandwidth
- $e_{\text{scatter}}(f)$ is significantly frequency-dependent, as one would expect due to the superposition of scattering contributions from an electrically large structure

$$e_{\text{scatter},\text{sim}}(f) = \frac{E_{\text{scatter},\text{sim}}(f)}{E_{\text{init},\text{sim}}}$$

Representation of Pulse Forms in Time Domain

Arbitrary Electromagnetic Pulse

can be described as real part of:

$$\mathbf{E}(t) = [\mathbf{e}_v A_v(t) + \mathbf{e}_h A_h(t)] e^{j2\pi f_0 t}$$

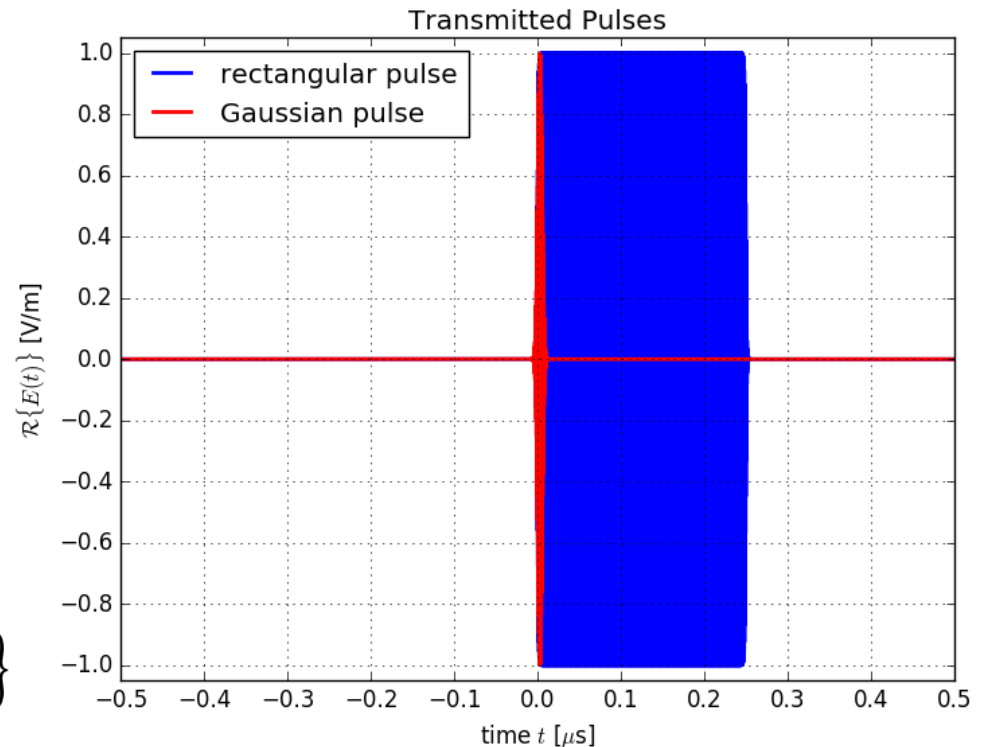
$A_i(t)$ [V/m] is the complex, time dependent envelope of the pulse

Gaussian Pulse:

$$A_{\text{gauss}}(t) = A_0 e^{-\frac{(t-t_{\text{pulse}})^2}{2\sigma_{\text{gauss}}^2}}$$

Smoothed Rectangular Pulse:

$$A_{\text{rect}}(t) = A_0 \left\{ \frac{1}{2} \left[1 + \tanh \left(\frac{t-t_{\text{rise}}}{T_{\text{rise}}} \right) \right] - \frac{1}{2} \left[1 + \tanh \left(\frac{t-t_{\text{fall}}}{T_{\text{fall}}} \right) \right] \right\}$$



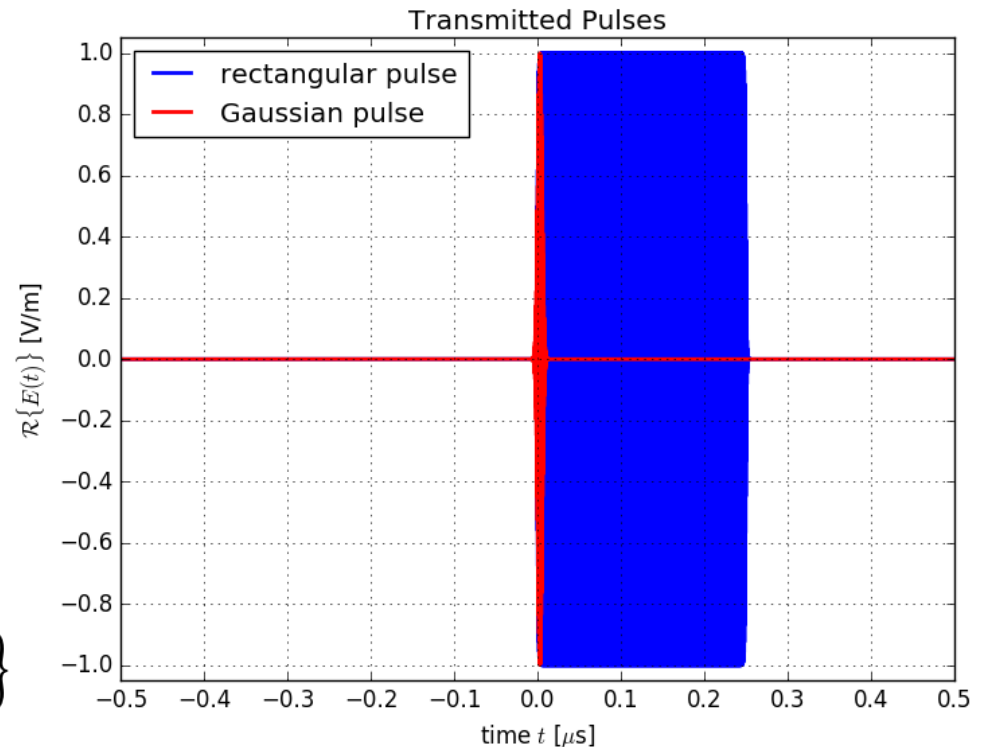
Representation of Pulse Forms in Time Domain

Gaussian Pulse:

$$A_{\text{gauss}}(t) = A_0 e^{-\frac{(t-t_{\text{pulse}})^2}{2\sigma_{\text{gauss}}^2}}$$

Smoothed Rectangular Pulse:

$$A_{\text{rect}}(t) = A_0 \left\{ \frac{1}{2} \left[1 + \tanh \left(\frac{t-t_{\text{rise}}}{T_{\text{rise}}} \right) \right] - \frac{1}{2} \left[1 + \tanh \left(\frac{t-t_{\text{fall}}}{T_{\text{fall}}} \right) \right] \right\}$$



Arbitrary choice of parameters (to showcase pertinent effects):

$T_{\text{rise}} = 1.25 \mu\text{s}$, pulse duration: 2.5 ns (Gauss pulse), 0.25 μs (rectangular pulse)

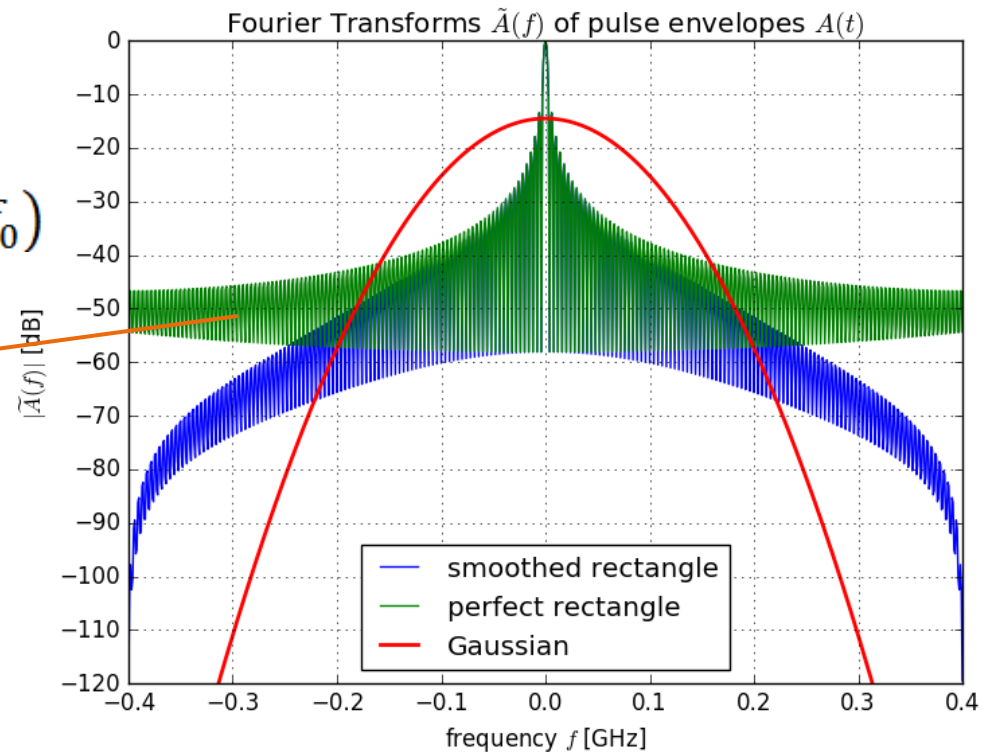
Bandwidth 0.8 GHz, $\Delta f = 1 \text{ MHz}$, $T = 1 \mu\text{s}$

Transformation of Pulses to Frequency Domain

Fourier Transform of Electric Field:

$$F\{E(t)\} = \tilde{A}(f) * \delta(f-f_0) = \tilde{A}(f-f_0)$$

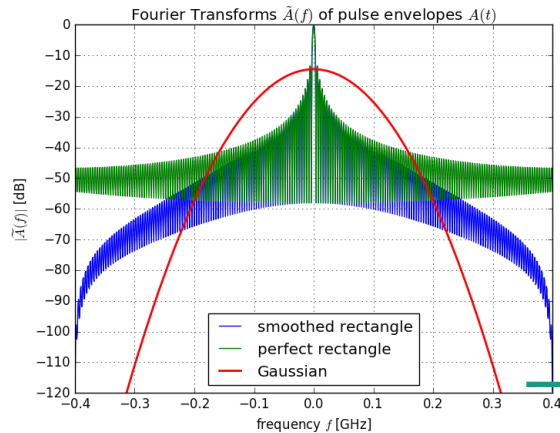
Perfect rectangular pulse for comparison



After Fourier Transformation:

- Cut spectrum according to bandwidth of simulated data
- Might lead to inaccuracy if pulse has significant contributions out of simulated band

Transformation back to Time Domain (1)

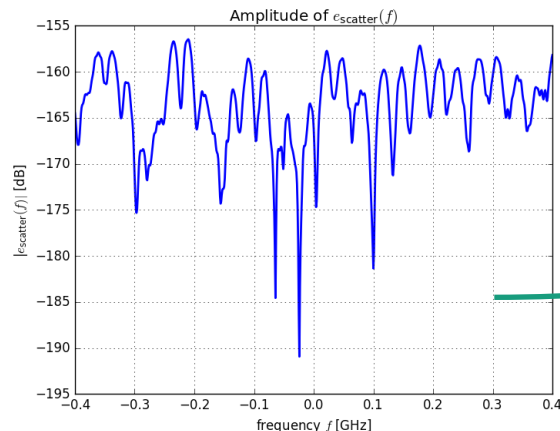


In frequency domain, the Fourier Transform of the pulse envelope is multiplied with the down-converted scattering results from the ray tracing simulation

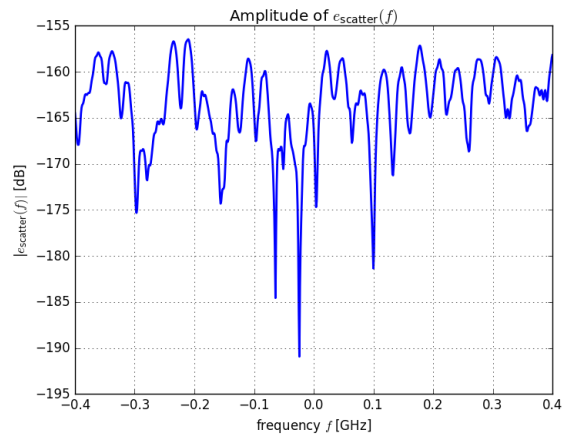
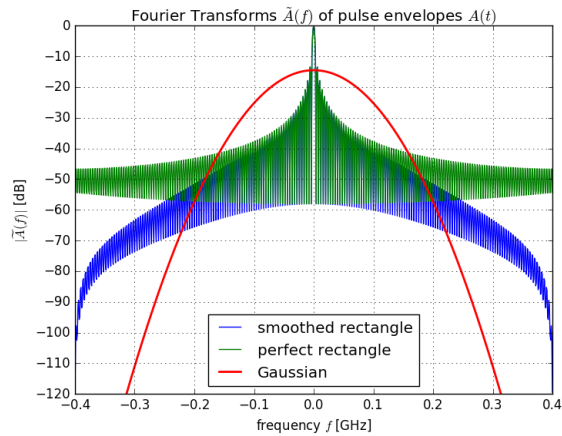
Scattered Pulse in Time Domain:

$$E_{\text{scatter}}(t) = F^{-1}\{e_{\text{scatter, sim}}(f + f_0)\tilde{A}(f) * \delta(f - f_0)\}$$

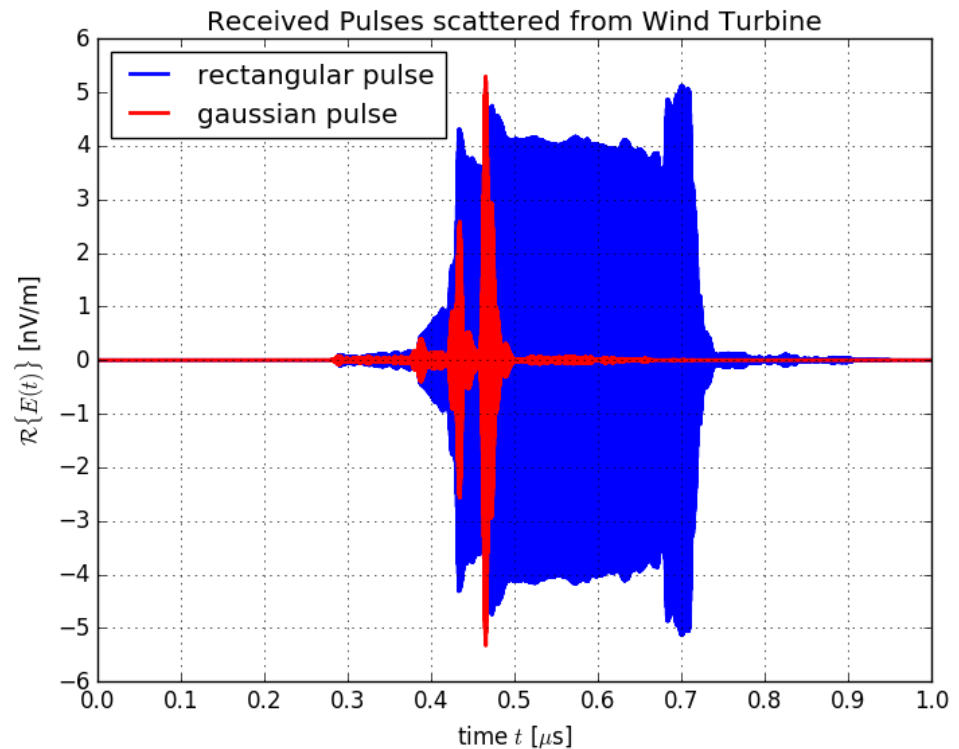
$$= F^{-1}\{e_{\text{scatter, sim}}(f + f_0)\tilde{A}(f)\}e^{j2\pi f_0 t}$$



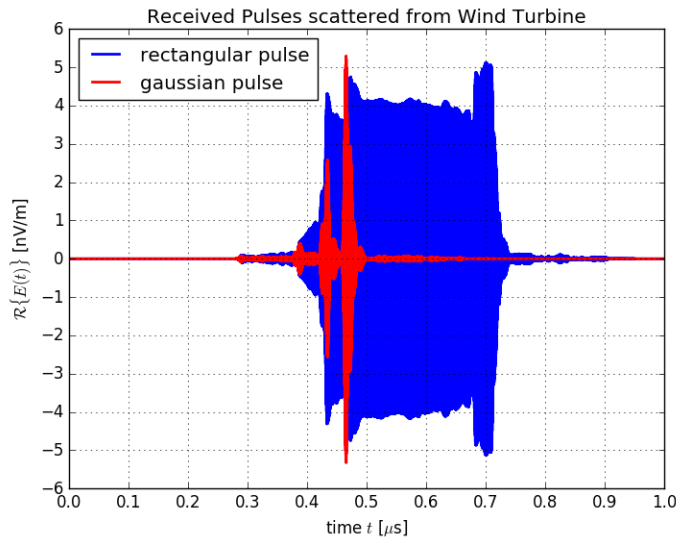
Transformation back to Time Domain (2)



Scattered Pulse in Time Domain:

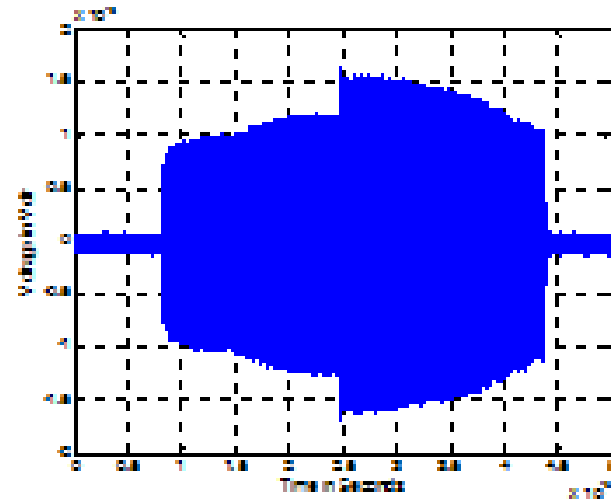


How to Compare Simulated and Measured Data (2)



Simulated Data:

- Scattered pulse in **time domain**
- Time domain post-processing can be done for arbitrary pulses without the need of repeating the simulation for each pulse



Measured Data:

- Pulse modulation in **time domain**

Summary

- Measurements:
Fluctuations in the order of several dB are to be expected for the electromagnetic fields behind wind farms
- EM Simulations:
Frequency Domain Simulations; Studies of Time Variance:
Good qualitative agreement with measurements
- Modelling of Scattered Pulses in Time Domain
Broadband frequency domain simulation of scattered fields
Multiplication with Fourier Transform of pulse
Transformation back to time domain
Time domain post-processing for arbitrary pulses

Literature

- F. Weinmann, J. G. Worms, P. Knott, "The Influence of Time-Variant Propagation Effects due to Rotating Wind Turbines," 2017 European Radar Conference (EuRAD), 9-13 October 2017, Nuremberg, Germany.
- F. Weinmann, "EM Modelling of Radar Signatures of Targets Behind Wind Farms – A Time-Gating Ray Tracing Approach," 2016 European Radar Conference (EuRAD), 3-7 October 2016, London, UK.
- F. Weinmann, J. G. Worms, "EM Scattering Effects Caused by Wind Turbines," EuCAP 2016 10th European Conference on Antennas and Propagation, 10-14 April 2016, Davos, Switzerland.
- F. Weinmann, J. G. Worms, "Time-Variant Scattering Properties of Wind Turbines," EuCAP 2015 9th European Conference on Antennas and Propagation, 13-17 April 2015, Lisbon, Portugal.
- F. Weinmann, "High-Frequency Electromagnetic Simulation of Wind Turbines in Realistic Scenarios and Approximation Techniques for Reducing the Complexity of Computations," 9th Future Security 2014, 16-18 September 2014, Berlin, Germany.
- F. Weinmann, "Accurate Prediction of EM Scattering by Wind Turbines," EuCAP 2014 8th European Conference on Antennas and Propagation, 6-11 April 2014, The Hague, The Netherlands.